

TECHNICAL MEMORANDUM

November 6, 2024

- To: Union County Board of County Commissioners 500 N. Main Street, Suite 932 Monroe, NC 28112
- From: BGE, Inc., on behalf of D.R. Horton, Inc. 1111 Metropolitan Ave, Suite 250 Charlotte, NC 28204

RE: Project 20222058 – Sanctuary at Southgate Phase II Development Pump Station Alternatives Analysis

Dear Board of Commissioners,

BGE, Inc. (BGE), on behalf of D.R. Horton, Inc., completed the pump station alternatives analysis for the proposed Sanctuary at Southgate Phase II development to garner your approval for a new pump station. The proposed Sanctuary at Southgate Phase II development is located in Union County, North Carolina, at the intersection of Poplin Road and North Rocky River Road (See Appendix 1) and is comprised of 75 single-family residential homes, a future mixed use development with multi-family units, clubhouse and pool, a future commercial development with mixed use retail shops, fast food restaurant, medical office, grocery, coffee shop, fuel center, car wash, restaurant, and a future fire station. The proposed development is within Union County's Twelve Mile Creek Water Reclamation Facility's service area via the Poplin Road Pump Station.

D.R. Horton, Inc., in collaboration with Walton Global Holdings, LLC, has reviewed the Future Land Use Plans for Union County and Indian Trail and believe the proposed pump station is well-suited for the larger goals of the municipality and the county. The Town of Indian Trail 2041 Future Land Use Plan, adopted 7/12/2022, identifies this area as a Walkable Activity Center. A Walkable Activity Center is home to a broad range of uses including commercial, office, and residential with an emphasis on promoting economic development.

The Union County 2050 Comprehensive Plan shows this area located in proximity to Community and Employment Centers located off Unionville-Indian Trail Road and the Monroe Expressway. D.R. Horton, Inc. and Walton Global Holdings, LLC believe a regional pump station fits both the economic goals of Indian Trail and Union County based on the planning and plans.

Walton Global Holdings, LLC donated land to Indian Trail that has been identified for a future Fire Station. The funding for the Fire Station is discussed in the Union County Capital Improvement Plan and the proposed pump station would service the facility.

This Technical Memorandum outlines the proposed project, potential area to be served by the pump station, capacity analyses completed by Black & Veatch, and the pump station alternatives analysis with life cycle cost calculations. The pump station alternatives analysis compares Alternative 1, including a proposed new on-site pump station with force main connecting to the existing gravity sewer infrastructure of the Annandale Subdivision, and Alternative 2, including a proposed gravity

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sewer main connecting to the Porter Ridge Pump Station (See Appendix 7). For Alternative 2, Black & Veatch completed an analysis outlining required upgrades to the existing Porter Ridge and Fieldstone Pump Stations.

The life cycle costs analysis determined the proposed Alternative 1 is more cost effective than Alternative 2 (See Total Life Cycle Cost Alternative Summary Table).

Total Life Cycle Cost Alternative Summary Table - NPV		
Alternative 1 - On-Site Pump Station with Gravity Sewer Connection at Annandale Subdivision	\$2,086,600.86	
Alternative 2 - Off-Site Gravity Sewer Connection to Porter Ridge Pump Station	\$3,585,319.06	
DELTA	\$1,498,718.20	

Based on the life cycle cost analysis for both pump station alternatives, a new on-site pump station receiving wastewater flows from the proposed Sanctuary at Southgate Phase II development with connection to existing gravity sewer infrastructure of the Annandale subdivision, would be the best option for this project.

Please contact me (msinkovitz@bgeinc.com; 980.867.4497) with any questions or concerns.

Thank-you for your consideration.

Sincerely,

Mathew J. Si 11/06/2024

Matthew J. Sinkovitz, P.E. Senior Project Manager



TABLE OF CONTENTS

	1
BACKGROUND	1
ALTERNATIVE 1 – ON-SITE PUMP STATION WITH GRAVITY SEWER CONNECTION AT ANNANDALE SUBDIVISION	3
ALTERNATIVE 2 – OFF-SITE GRAVITY SEWER CONNECTION TO PORTER RIDGE PUMP STATION	4
CONCLUSION	5

APPENDICES

- APPENDIX 1 SITE LOCATION MAP
- APPENDIX 2 PROPOSED PUMP STATION SERVICE AREA MAP
- APPENDIX 3 UTILITY SKETCH PLAN, DATED 10/10/2024
- APPENDIX 4 BGE PROPOSED PUMP STATION PEAK WET WEATHER SEWER FLOW
- APPENDIX 5 BLACK & VEATCH SANCTUARY AT SOUTHGATE PHASE 2 WASTEWATER COLLECTION SYSTEM ANAYLYSIS, DATED 4/26/2023
- APPENDIX 6 BLACK & VEATCH SANCTUARY AT SOUTHGATE PHASE 2 REVISED WASTEWATER COLLECTION SYSTEM ANALYSIS, DATED 8/24/2023
- APPENDIX 7 PUMP STATION ALTERNATIVES
- APPENDIX 8 BLACK & VEATCH SANCTUARY AT SOUTHGATE GRAVITY ALTERNATIVE CALCULATIONS, DATED 11/21/2023
- APPENDIX 9 NEW SANCTUARY AT SOUTHGATE PHASE II PUMP STATION CALCULATIONS
- APPENDIX 10 NEW SANCTUARY AT SOUTHGATE PHASE II PUMP STATION FLYGT NP 3127 PUMP
- APPENDIX 11 ALTERNATIVE 1 LIFE CYCLE COST ANALYSIS
- APPENDIX 12 BGE PORTER RIDGE PUMP STATION CALCULATIONS
- APPENDIX 13 BGE FIELDSTONE PUMP STATION CALCULATIONS
- APPENDIX 14 PORTER RIDGE PUMP STATION FLYGT NP 3153 PUMP
- APPENDIX 15 FIELDSTONE PUMP STATION FLYGT NP 3202.185 HT PUMP
- APPENDIX 16 ALTERNATIVE 2 LIFE CYCLE COST ANALYSIS

INTRODUCTION

D.R. Horton and Walton Global Holdings, LLC (Walton) are seeking Union County Board of County Commissioners approval for the Sanctuary at Southgate Phase II development. The project is located in Union County, North Carolina, at the intersection of Poplin Road and North Rocky River Road (See Appendix 1). The Phase II site includes a portion of parcel 07006001A, 07021015E, parcel 07009017, parcel 07006001B, and parcel 07009017A, totaling 61.2 acres (See Appendices 1 and 2). The Phase II development includes 75 single-family residential homes (by D.R. Horton), a future multi-family development including 240 multi-family units (by Walton), a future commercial development including a shopping center with food service (by others), with sanitary sewer infrastructure including gravity lines, on-site pump station, and force main. Walton has started preliminary design on the commercial components and is actively marketing the spaces to well-known retailers. BGE prepared this Pump Station Alternatives Analysis to meet the requirements of Union County Code, Section 34-336, Para b.1.b. The analysis includes the (1) area to be served by the proposed pump station, (2) volume of wastewater flow to be generated by the development, (3) capacity analysis with necessary improvements identified to handle flow from the development, and (4) a pump station alternative analysis comparing the lifecycle costs of gravity and pump station sanitary sewer solutions for the development.

BACKGROUND

The area to be served by the proposed pump station totals approximately 74 acres and includes 75 singlefamily residential homes (by D.R. Horton), a future multi-family development (by Walton), two future commercial developments (by others), and a future emergency response facility (by others) (See Appendix 2). The Utility Sketch Plan developed by BGE is included as Appendix 3.

BGE determined the total wastewater demand of the proposed Sanctuary at Southgate Phase II development and the future multi-family, commercial, and the future emergency response facility serviced by the proposed pump station to be **97,870 GPD** (See Appendix 4). BGE utilized the total wastewater demand and determined the total peak wet weather wastewater flow design condition for the proposed pump station to be **177.20 GPM**, by applying the minimum peaking factor of 2.5 as outlined in the *NCDENR Minimum Design Criteria for the Permitting of Pump Stations and Force Mains* to all design daily flows, except the single family detached lots (See Appendix 4). BGE applied a peaking factor of 3 to the single family detached lots design daily flow per Black & Veatch's assumptions outlined in its Sanctuary at Southgate Phase 2 Wastewater Collection System Analyses (See Appendices 5 & 6).

Black & Veatch analyzes wastewater flows and provides wastewater collection system hydraulic modeling services for Union County Water (UCW). Black & Veatch completed two (2) Sanctuary at Southgate Phase II wastewater collection system analyses to determine impacts of the new development on wastewater flows in the receiving wastewater collection system.

Black & Veatch's first analysis, dated 4/26/2023 (See Appendix 5), analyzed two alternatives.

- Alternative 1 On-Site Pump Station with Gravity Sewer Connection at Phase I. Alternative 1 includes an on-site pump station for the Sanctuary at Southgate Phase II development with force main discharging into the gravity sewers installed during the Sanctuary at Southgate Phase I development. "After being discharged to the Phase 1 sewer, wastewater will flow downstream by gravity to an existing 12-inch sewer. The flow travels through 5,200 feet of 12-inch sewer, the Fieldstone Pump Station, and 4,500 feet of 6-inch force main and then discharges to 1,300 feet of 8-inch gravity sewer that flows to the Poplin Road Pump Station" (Black & Veatch, 4/26/2023).
- Alternative 2 Off-Site Gravity Sewer Connection to Porter Ridge Pump Station. Alternative 2 assumes construction of 4,700 feet of adequately sized sewer to convey project flows to the Porter Ridge service area. Sanctuary at Southgate Phase II development wastewater flows "would connect to a 3,100 LF 8inch gravity sewer leading to the Porter Ridge pump station, which discharges into the 12-inch

Fieldstone service area collection sewer, approximately 8,000 LF downstream of the connection point indicated on the development's site utility plan" (Black & Veatch, 4/26/2023).

The findings and recommendations outlined in Black & Veatch's report, dated 4/26/2023, include:

- Evaluation of both the 12-inch and 8-inch gravity sewers associated with the Sanctuary at Southgate Phase II Development flows determined neither are predicted to surcharge under a 1-year storm event.
- Alternative 2 "has little effect on the analysis in terms of capacity based on the modeling results but requires the construction of off-site gravity sewer conveying flows to the Porter Ridge Pump Station service area. The Porter Ridge Pump Station capacity needs to be evaluated if [Alternative 2] is further considered."
- The allocation and firm capacities of the Fieldstone Pump Station are exceeded with the addition of the Sanctuary at Southgate Phase II development wastewater flows. "It is not recommended that the 0.44 MGD firm capacity of the [Fieldstone Pump Station] be exceeded."
- The allocation and firm capacities of the Poplin Road Pump Station are exceeded with the addition of the Sanctuary at Southgate Phase II development wastewater flows. "Approval for this development is dependent on completion of the CIP improvement project that will install adequate flow equalization at the Poplin Road Pump Station. Once an equalization tank is installed, the storage volume will be sufficient to prevent backup in the gravity system upstream of the Poplin Pump Station." [Per email from Crystal Panico, dated 12/7/2023, the equalization tank was substantially completed and should be online in the next couple of months.]
- "The Twelve Mile Creek WRF has a rated capacity of 7.5 MGD."

At Union County Water's direction, Black & Veatch analyzed two additional alternatives and issued a Sanctuary at Southgate Phase 2 Revised Wastewater Collection System Analysis, dated 8/24/2023 (See Appendix 6).

- Alternative 3 On-Site Pump Station with Gravity Sewer Connection at Sedgewick Road. Alternative 3
 includes an on-site pump station for the Sanctuary at Southgate Phase II development with force main
 discharging to the northwest, across Poplin Road, into the gravity sewer along <u>Sedgewick Road</u>, and
 the gravity sewer conveying wastewater flow approximately 2,000 feet to the Poplin Road Pump
 Station.
- Alternative 4 On-Site Pump Station with Gravity Sewer Connection at Potomac Road. Alternative 4
 includes an on-site pump station for the Sanctuary at Southgate Phase II development with force main
 discharging to the northwest, across Poplin Road, into the gravity sewer along <u>Potomac Road</u>, and the
 gravity sewer conveying flow approximately 2,000 feet to the Poplin Road pump station.

The findings and recommendations outlined in Black & Veatch's report, dated 8/24/2023, include:

- Both Alternative 3 and Alternative 4 "are not predicted to surcharge under a 1-year storm event." Either sewer discharge location "is viable from a capacity standpoint."
- "The allocation and firm capacities of the Poplin Road Pump Station are exceeded with the addition of [the Sanctuary at Southgate Phase II development] proposed peak flows."
- "Approval for [the Sanctuary at Southgate Phase II development] is dependent on completion of the CIP improvement project that will provide flow equalization at the Poplin Road Pump Station. At that point, the storage volume will be sufficient to prevent backup in the gravity system upstream of the Poplin Road Pump Station...Until the Poplin Road Pump Station [Equalization] Basin project is completed, it is not recommended that the 3.64 MGD operational capacity of the station be exceeded." [Per email from Crystal Panico, dated 12/7/2023, the equalization tank was substantially completed and should be online in the next couple of months.]
- "The Twelve Mile Creek WRF has a rated capacity of 7.5 MGD."

Based on the analyses completed by Black & Veatch, topography, and direction provided by UCW [Per email from Crystal Panico, dated 9/29/2023), BGE defined two alternatives for the Pump Station Alternatives Analysis. Alternative 1 includes an on-site pump station with gravity sewer force main connecting to existing infrastructure at Potomac Road (Annadale Subdivision) and Alternative 2 includes gravity sewer line connecting to the Porter Ridge Pump Station with upgrades to the existing Porter Ridge Pump Station and the Fieldstone Pump Station (See Appendix 7). For Alternative 2, Black & Veatch outlined the required upgrades for the existing Porter Ridge Pump Station and the Fieldstone Pump Station (See Appendix 7). For Alternative 2, Black & Veatch outlined the required upgrades for the existing Porter Ridge Pump Station and the Fieldstone Pump Station in the Sanctuary at Southgate Gravity Alternative Calculations, dated 11/21/2023 (See Appendix 8). Black & Veatch recommended the following for Alternative 2:

- Minimum 8-inch pipe diameter for the 7,100 linear feet of gravity sewer.
- Replace the two (2) pumps at the Porter Ridge Pump Station pumps with 275 GPM pumps at 105 feet of head.
- Replace the two (2) pumps at the Fieldstone Pump Station with news pumps at design point of 490 GPM at approximately 102 feet of head.
- "The pump sizing at each station is increasing by [30% to 50%]. Wet well improvements may be
 required depending on size of [the] new pumps and [the] existing wet well." Wet wells should be
 assessed to ensure the pumps fit in the pump slots and the wet well provides adequate volume to limit
 the number of on/off cycles. "The sizing of the existing electrical systems and generator should also be
 assessed to determine whether they can support the larger pumps."

ALTERNATIVE 1 – ON-SITE PUMP STATION WITH GRAVITY SEWER CONNECTION AT ANNANDALE SUBDIVISION

Overview

Alternative 1 includes a new on-site pump station for the proposed Sanctuary at Southgate Phase II development and 5,460 linear feet of 6" PVC sanitary sewer force main connecting to existing sanitary sewer infrastructure at Potomac Road (See Appendix 7).

Assumptions

- BGE calculated a total sewer demand of 97,870 GPD (design daily flow = 67.97 GPM) and utilized a 2.5 peaking factor per NCDENR Minimum Design Criteria for the Permitting of Pump Stations and Force Mains, except for the single family detached lots. BGE applied a peaking factor of 3 to the single family detached lots design daily flow per Black & Veatch's assumptions outlined in its Sanctuary at Southgate Phase 2 Wastewater Collection System Analyses (See Appendices 5 & 6). This resulted in a peak wet weather wastewater flow of 255,175 GPD (peak hourly flow = 177.20 GPM) (See Appendix 4).
- New Sanctuary at Southgate Phase II pump station calculations are included as Appendix 9.
- BGE coordinated pump recommendations with Xylem Water Solutions USA, Inc. (Xylem). For the pump station condition of pump rate = 225 GPM, static head = 43 feet, and total head = 64 feet, Xylem recommended the Flygt NP 3127 HT 3~ Adaptive 488 pump (See Appendix 10).
- BGE coordinated pump station budget costs with CMH Solutions, LLC (CMH). CMH provided a lump sum budget cost of **\$963,000** for the new on-site Sanctuary at Southgate Phase II pump station. Scope included:
 - o 6-foot diameter, 21-foot deep wet well,
 - 4-inch discharge piping and 4-inch valve vault piping (force main will increase to 6-inch after the valve vault),
 - One (1) 8-inch gravity sewer into the wet well, and
 - o 30-foot driveway.

Life Cycle Cost Analysis

BGE completed a life cycle cost analysis per the Union County Water Documentation Requirements for the Consideration of Wastewater Pump Stations. BGE determined the Net-Present-Value of Alternative 1 lifecycle costs is **\$2,086,600.86** (See Appendix 11).

ALTERNATIVE 2 – OFF-SITE GRAVITY SEWER CONNECTION TO PORTER RIDGE PUMP STATION

Overview

Alternative 2 includes construction of 7,100 linear feet of 8" PVC gravity sewer line with upgrades to the existing Porter Ridge Pump Station and the Fieldstone Pump Station.

Assumptions

- For the Porter Ridge Pump Station, BGE estimated a total sewer demand of 151,570 GPD (design daily flow = 105.26 GPM) and utilized a 2.5 peaking factor per NCDENR Minimum Design Criteria for the Permitting of Pump Stations and Force Mains, except for the single family detached lots. BGE applied a peaking factor of 3 to the single family detached lots design daily flow per Black & Veatch's assumptions outlined in its Sanctuary at Southgate Phase 2 Wastewater Collection System Analyses (See Appendices 5 & 6). This resulted in a peak wet weather wastewater flow of 389,425 GPD (peak hourly flow = 270.43 GPM). Porter Ridge Pump Station calculations are included as Appendix 12.
- For the Fieldstone Pump Station, BGE estimated a total sewer demand of 310,050 GPD (design daily flow = 215.31 GPM) and utilized a 2.5 peaking factor per NCDENR Minimum Design Criteria for the Permitting of Pump Stations and Force Mains, except for the single family detached lots. BGE applied a peaking factor of 3 to the single family detached lots design daily flow per Black & Veatch's assumptions outlined in its Sanctuary at Southgate Phase 2 Wastewater Collection System Analyses (See Appendices 5 & 6). This resulted in a peak wet weather wastewater flow of 785,625 GPD (peak hourly flow = 545.57 GPM). Fieldstone Pump Station calculations are included as Appendix 13.
- BGE coordinated pump recommendations with Xylem for the Porter Ridge Pump Station. For the pump station condition of pump rate = 300 GPM, static head = 43 feet, and total head = 94 feet, Xylem recommended the Flygt NP 3153 HT 3~ 462 pump (See Appendix 14).
- BGE coordinated Porter Ridge Pump Station upgrade budget costs with CMH Solutions, LLC (CMH). CMH provided a lump sum budget cost of \$430,000 for the Porter Ridge Pump Station upgrades. Scope included:
 - Replace existing pumps with two (2) new Flygt NP 3153 HT 3~ 462 pumps,
 - Modifications to the existing pump control panel to include new 30Hp solid state reduced voltage starters, pump breakers, transformer breaker, power wiring, and ancillary controls as required,
 - o Replace existing generator with a 60kW unit with 80kW alternator and 200A transfer switch, and
 - Upgrade existing electrical service to a 200A service.
 - The budget cost includes by-pass operations for the duration of the system upgrade.
 - The budget cost does not include modifications to the existing Radio Telemetry System.
- BGE coordinated pump recommendations with Xylem for the Fieldstone Pump Station. For the pump station condition of pump rate = 600 GPM, static head = 62 feet, and total head = 167 feet, Xylem recommended the Flygt NP 3202.185 HT pump (See Appendix 15).
- BGE coordinated Fieldstone Pump Station upgrade budget costs with CMH Solutions, LLC (CMH). CMH provided a lump sum budget cost of \$642,000 for the Fieldstone Pump Station upgrades. Scope included:
 - Replace existing pumps with two (2) new Flygt NP 3202.185 HT pumps,
 - Modifications to the existing pump control panel to include new 75Hp solid state reduced voltage starters, pump breakers, transformer breaker, power wiring, and ancillary controls as required,

- Replace existing generator with a 175kW unit with 200kW alternator and 400A transfer switch, and
- Upgrade existing electrical service to a 400A service.
- The budget cost includes by-pass operations for the duration of the system upgrade.
- The budget cost does not include modifications to the existing Radio Telemetry System.
- BGE assumed construction of a 7,100 linear foot 8" PVC gravity sanitary sewer line with manholes located every 425 feet (plus 20%, one at beginning, and one at end).
- BGE assumed 10 acres of clearing and grubbing would be required to construct the new gravity sanitary sewer line.
- BGE assumed 10 acres of temporary construction easement and five (5) acres of sanitary sewer easement would be acquired for the new gravity sanitary sewer line.

Life Cycle Cost Analysis

BGE completed a life cycle cost analysis per the Union County Water Documentation Requirements for the Consideration of Wastewater Pump Stations. BGE determined the Net-Present-Value of Alternative 2 lifecycle costs is **\$3,585,319.06** (See Appendix 16).

CONCLUSION

The life cycle cost analysis determined Alternative 1 is more cost effective than Alternative 2.

Total Life Cycle Cost Alternative Summary Table - NPV		
Alternative 1 - On-Site Pump Station with Gravity Sewer Connection at Annandale Subdivision	\$2,086,600.86	
Alternative 2 - Off-Site Gravity Sewer Connection to Porter Ridge Pump Station	\$3,585,319.06	
New Gravity Sanitary Sewer Line	\$1,669,354.47	
Porter Ridge Pump Station Upgrades	\$753,607.36	
Fieldstone Pump Station Upgrades	\$1,162,357.23	
DELTA	\$1,498,718.20	

APPENDIX 1 - SITE LOCATION MAP



APPENDIX 2 - PROPOSED PUMP STATION SERVICE AREA MAP







PUMP STATION SERVICE AREA (+/- 61.2 ACRES)

PARCELS: 07006001A 07006001B 07009017 07009017A 07021007A 07021007J 07021015E

CALCULATIONS:

IRRIGATION WATER USAGE:

SINGLE FAMILY RESIDENTIAL UNITS 75 RESIDENTIAL UNITS X 200 GPD/LOT = 15,000 GPD

OPEN SPACE - MULTI-FAMILY / AMENITY AREA 6,250 CU. FT X 7.48052 GAL/CU. FT = 46,754 GAL/WK = 6,679 GPD ASSUMES 1/2" WATERING WEEKLY ON APPROX. 150,000 SF OF LANDSCAPED AREAS. 1/2" = 0.041667 FT

TOTAL IRRIGATION WATER DEMAND = 21,679 GPD

DOMESTIC WATER USAGE:

SINGLE FAMILY RESIDENTIAL UNITS 75 RESIDENTIAL UNITS X 400 GPD = 30,000 GPD

FUTURE MULTI-FAMILY DEVELOPMENT UNITS (240 UNITS, ASSUME 3 BEDROOMS PER UNIT): 720 BEDROOMS X 125 GPD/BEDROOM = 90,000 GPD CLUBHOUSE:10 FIXTURES X 250 GPD/FIXTURE = 2,500 GPD POOL: 2,500 SF / 15 POOL SURFACE AREA SF/SWIMMER = 167 SWIMMERS 10 GPD/SWIMMER X 167 SWIMMERS = 1,670 GPD

REQUESTED DOMESTIC WATER DEMAND = 124,170 GPD PEAK DOMESTIC WATER DEMAND = 215.6 GPM

DOMESTIC WASTEWATER DEMAND FLOW:

SINGLE FAMILY RESIDENTIAL UNITS 75 RESIDENTIAL UNITS X 280 GPD = 21,000 GPD

FUTURE MULTI-FAMILY DEVELOPMENT UNITS (240 UNITS, ASSUME 3 BEDROOMS PER UNIT): 720 BEDROOMS X 70 GPD/BEDROOM = 50,400 GPD CLUBHOUSE: 10 FIXTURES X 250 GPD/FIXTURE = 2,500 GPD POOL: 2,500 SF / 15 POOL SURFACE AREA SF/SWIMMER = 167 SWIMMERS 10 GPD/SWIMMER X 167 SWIMMERS = 1,670 GPD

TOTAL DOMESTIC WASTEWATER DEMAND = 75,570 GPD

COMMERCIAL WATER USAGE AND WASTEWATER DEMAND FLOW: (PEAK FLOWS CALCULATED USING 2.5 PEAKING FACTOR)

FUTURE EMERGENCY RESPONSE BUILDING (BY OTHERS) 10 FIXTURES X 250 GPD/FIXTURE = 2,500 GPD PEAK = 4.34 GPM

FUTURE COMMERCIAL DEVELOPMENT

GROCERY CENTER (75,000 SF) DELI = 1,000 SF X 40 GPD/100 SF = 400 GPD MEAT/FISH DEPARTMENT = 2,000 SF X 75 GPD/100 SF = 1,500 GPD 16 FIXTURES X 250 GPD/FIXTURE = 4,000 GPD TOTAL = 5,900 GPD PEAK = 10.24 GPM

COFFEE SHOP WITH DRIVE THROUGH (10,000 SF) 10,000 SF X 50 GPD/100 SF = 5,000 GPD PEAK = 8.68 GPM FUEL CENTER (9,500 SF) 2 FIXTURES X 250 GPD/FIXTURE = 500 GPD PEAK = 0.87 GPM CAR WASH (5,000 SF) 1,200 GPD/BAY X 2 BAYS = 2,400 GPD PEAK = 4.17 GPM RESTAURANT (150 SEATS) (BY OTHERS)

40 GAL/SEAT X 200 SEATS = 6,000 GPD PEAK = 10.42 GPM

TOTAL COMMERCIAL WASTEWATER DEMAND = 22,300 GPD TOTAL COMMERCIAL WATER DEMAND = 22,300 GPD PEAK COMMERCIAL WATER DEMAND = 38.7 GPM

CALCULATIONS SUMMARY

WATER DEMAND SUMMARY (PS SERVICE AREA)				
DEMAND TYPE	FLOW	UNIT		
IRRIGATION	21,679	GPD		
DOMESTIC	124,170	GPD		
COMMERCIAL	22,300	GPD		
TOTAL	168,149	GPD		
PEAK DOMESTIC	216	GPM		
PEAK COMMERCIAL	38.7	GPM		
TOTAL	254	GPM		

WASTEWATER DEMAND SUMMARY (PS SERVICE AREA)				
DEMAND TYPE	FLOW	UNIT		
DOMESTIC	75,570	GPD		
COMMERCIAL	22,300	GPD		
TOTAL	97,870	GPD		



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APPENDIX 4 - BGE PROPOSED PUMP STATION PEAK WET WEATHER SEWER FLOW

ESTIMATED DOMESTIC SEWER DEMAND				
SANCTUARY	SANCTUARY AT SOUTHGATE PHASE II SINGLE FAMILY DETACHED LOTS			
TOTAL (LOTS)	GPD/LOT	AVE DAILY FLOW (GPD)	PEAK WET WEATHER FLOW (GPD)	
75	280	21000	63000	
	FUTURE MULTI-FAMILY (BY OTHERS	UNITS (240) S)		
TOTALGPD/AVE DAILY FLOWPEAK WET(BEDROOMS)BEDROOM(GPD)(GPD)				
720	70	50400	126000	
FUTURE CLUBHOUSE (BY OTHERS)				
TOTAL (FIXTURES) GPD/ FIXTURE AVE DAILY FLOW WEA		PEAK WET WEATHER FLOW (GPD)		
10	250	2500	6250	
FUTURE POOL (BY OTHERS)				
TOTAL (SF)	SWIMMERS	AVE DAILY FLOW (GPD)	PEAK WET WEATHER FLOW (GPD)	
2500	167	1670	4175	
	TOTAL DOMESTIC SEWER	75570	199425	

NOTES:

1) WASTEWATER DESIGN FLOW RATES USED FROM 15A NCAC 02T .0114. 2A) 2500 SF / 15 POOL SURFACE AREA SF/SWIMMER = 167 SWIMMERS 2B) 10 GALLONS/DAY/SWIMMER

3) BGE UTILIZED MINIMUM PEAKING FACTOR OF 2.5 TO CALCULATE PEAK WASTEWATER FLOWS FOR ANY PUMP STATION. PER NCDENR MINIMUM DESIGN CRITERIA FOR THE PERMITTING OF PUMP STATIONS AND FORCE MAINS, IN ALL INSTANCES, EXCEPT FOR THE SINGLE FAMILY DETACHED LOTS. BGE UTILIZED A PEAKING FACTOR OF 3 TO CALCULATE PEAK WASTEWATER FLOWS FOR THE SINGLE FAMILY DETACHED LOTS.

ESTIMATED COMMERCIAL SEWER DEMAND			
EMERGENCY RESPONSE BUILDING			
	(BY OTHERS	6)	
TOTAL (FIXTURES) GPD/ FIXTURE (GPD) AVE DAILY FLOW (GPD)		PEAK WET WEATHER FLOW (GPD)	
10	250	2500	6250
	FUTURE GROCERY ((BY OTHERS	75,000 SF) S)	
SPACE	GPD	AVE DAILY FLOW (GPD)	PEAK WET WEATHER FLOW (GPD)
DELI	400		
MEAT/FISH DEPARTMENT	1500	5900	14750
FIXTURES	4000		
	FUTURE COFFEE SHOP (BY OTHERS	P (10,000 SF) S)	
GPD/100 SF	GPD/100 SF 100 SF AVE DAILY FLOW (GPD)		PEAK WET WEATHER FLOW (GPD)
50	100	5000	12500
	FUTURE FUEL CENTEI (BY OTHERS	R (9,500 SF) S)	
TOTAL (FIXTURES)	GPD/ FIXTURE	AVE DAILY FLOW (GPD)	PEAK WET WEATHER FLOW (GPD)
2	250	500	1250
FUTURE CAR WASH (5,000 SF) (BY OTHERS)			
GAL/BAY BAYS AVE DAILY FLOW (GPD)		PEAK WET WEATHER FLOW (GPD)	
1200	2	2400	6000
	FUTURE RESTAURANT (BY OTHERS	(150 SEATS) S)	
GAL/SEAT	SEATS	TOTAL (GPD)	PEAK WET WEATHER FLOW (GPD)
40	150	6000	15000
TOTAL	COMMERCIAL SEWER (GPD)	22300	55750
NOTES: 1) DESIGN FLOW RATES FROM NCAC 02T .0114. 2) ASSUMES 1,000 SF DELI, 2,000 SF MEAT/FISH DEPARTMENT, AND 16 BATHROOM FIXTURES FOR GROCERY			
3) ASSUMES 200 SF PER EMPLOYEE FOR MIXED USE RETAIL SHOPS AND ONE SHIFT.			
A) ASSUMES 1 MEDICAL PRACTITIONER PER 1 000 SE OF MEDICAL OFFICE SPACE AND			

ONE SHIFT. 5) BGE UTILIZED MINIMUM PEAKING FACTOR OF 2.5 TO CALCULATE PEAK WASTEWATER FLOWS FOR ANY PUMP STATION. PER NCDENR MINIMUM DESIGN CRITERIA FOR THE PERMITTING OF PUMP STATIONS AND FORCE MAINS, IN ALL INSTANCES, EXCEPT FOR THE SINGLE FAMILY DETACHED LOTS. BGE UTILIZED A PEAKING FACTOR OF 3 TO

CALCULATE PEAK WASTEWATER FLOWS FOR THE SINGLE FAMILY DETACHED LOTS.		
TOTAL SEWER DEMAND (GPD)	97870	255175
TOTAL PEAK WET WEA	THER FLOW (GPM)	177.20



26 April 2023

Union County Water 500 N. Main Street, Suite 500 Monroe, NC 28112 Wastewater Collection System Analysis Sanctuary at Southgate Phase 2 Black & Veatch Project 175886.8058

Attention: Crystal Outlaw Panico, PE

BACKGROUND

Union County Water (UCW) has requested that Black & Veatch perform hydraulic analyses for the proposed Sanctuary at Southgate development utilizing UCW's collection system hydraulic model. The analyses are intended to evaluate the impacts of the new development on wastewater flows in the receiving collection system. The proposed Sanctuary at Southgate Phase 2 development would be tributary to the Poplin Road pump station, which pumps receiving flows into the Twelve Mile Creek Basin.

Additionally, UCW has requested that a capacity analysis be performed for the collection system from the development to the Poplin Road Pump Station, including gravity sewer and the Fieldstone PS. Several developments that are permitted to discharge to the same gravity sewer as Sanctuary at Southgate Phase 2 but do not yet have a sewer connection are incorporated into this analysis. This analysis is intended to evaluate the impacts of the new development on the wastewater flows in the receiving collection system

DEVELOPMENT OVERVIEW

Based on the Utility Sketch Plan document prepared by BGE, Inc, dated July 7, 2022 the site will consist of 75 single family homes, 240 three-bedroom multi-family units, one clubhouse and pool, 24,500 SF of commercial development, a 200 seat restaurant, and an emergency response building. The development is located south of the intersection of Poplin Road and North Rocky River Road. The site is ±72 acres and Figure 1 shows a plan view of the proposed development.



Figure 1 Development Overview

ESTIMATED DEVELOPMENT WASTEWATER FLOWS

The developer's sketch included an estimate of total average daily flow of 97,870 gpd for the development. Table 1 summarizes the development's wastewater flows. In addition to the average daily flow estimates provided by the developer, the peak wet weather flows were estimated using a peaking factor of 3 for single family homes and a peaking factor of 2.5 for multi-family homes and commercial. The peak flows incorporate an infiltration and inflow (I/I) flow component for the proposed development and is in line with the peaking factors observed in the UCW 2011 Comprehensive Master Plan I/I estimates for new developments.

Flow Source	Number of Units/Size	Unit	Unit Rates	Average Daily Flow (gpd)	Peak Wet Weather Flow (gpd)
Single Family Residential Units	75	Units	280	21,000	63,000
Multi-Family Units	720	Bedrooms	70	50,400	126,000
Pool	1	Unit	1,670	1,670	4,175
Clubhouse	10	Fixtures	250	2,500	6,250
Commercial / Retail	-	-	-	22,300*	55,750
Total 97,870 255,175					
*Total commercial / retail calcs on project utility plans page U1-0 (total of 22,300 gpd) do not match page U1-1 calculations (total of 24,300 gpd).					

Table 1 Sanctuary at Southgate Phase 2 Development Wastewater Flows Summary

DEVELOPMENT ANALYSIS

Figure 2 is a map of the project location and contains a red-dashed line indicating the wastewater flow path for the development. The development contains an on-site pump station on the southeast portion of the site, according to site utility plans. The pump station would pump flows from Phase 2 of the development and discharge to the north into the Sanctuary at Southgate Phase 1 gravity sewers. After being discharged to the Phase 1 sewer, wastewater will flow downstream by gravity to an existing 12-inch sewer. The flow travels through 5,200 feet of 12-inch sewer, the Fieldstone Pump Station, and 4,500 feet of 6-inch force main and then discharges to 1,300 feet of 8-inch gravity sewer that flows to the Poplin Road Pump Station.

Additionally, a separate flow path was analyzed for the Sanctuary at Southgate Phase 2 development, indicated in Figure 2 with a blue-dashed line. This alternate flow path does not require an on-site pump station, but instead assumes the construction of approximately 4,700 LF of adequately sized sewer to convey project flows to the Porter Ridge service area. In this alternative, development flows would connect to a 3,100 LF 8-inch gravity sewer leading to the Porter Ridge pump station, which discharges into the 12-inch Fieldstone service area collection sewer, approximately 8,000 LF downstream of the connection point indicated on the development's site utility plan.



Figure 2 Development Location and Flow Paths

An initial model run was performed to simulate existing 2015 conditions within the Twelve Mile Creek model network under the 2011 Comprehensive Master Plan design storm event, a 1- year SCS Type III storm with a 24-hour duration. The 2015 model run was then adjusted to include the new Sanctuary at Southgate Phase 2 development. The impact to the collection system was compared to the predevelopment conditions including the receiving gravity sewer and the downstream system. Permitted development flows, totaling 122,180 gpd, were included in the model tributary to the Fieldstone PS. Estimated flows for the proposed new development, totaling 97,870 gpd were added on top these permitted flows in the 2015 model flows.

DEVELOPMENT RESULTS

The Sanctuary at Southgate Phase 2 pump station would pump flows from the project site to the north into the Phase 1 gravity sewers. After being discharged to the Phase 1 sewer, wastewater will flow downstream by gravity to the existing 12-inch sewer. The 2015 model was updated to show the new development flows going to the indicated connection point. Model

flows were compared against the UCW criteria for improvements in the wastewater collection system. The criteria that would trigger an improvement in the UCW gravity sewers is 50% of the MH depth surcharged above the crown of the pipe during a 1-year design storm.

The model predicts there will be no surcharge in pipes downstream of the development, and the addition of the Sanctuary at Southgate Phase 2 development flow does not increase the peak flows significantly. The peak flow to the Fieldstone pump station is approximately 0.70 MGD, and the peak velocity in the force main is 5.38 ft/s. The peak flows from proposed and permitted developments exceed the station's firm capacity of 0.44 MGD. The peak flow to the Poplin Road pump station is 4.07 mgd; however, the firm pumping capacity of the Poplin Road pump station is limited to 3.64 mgd because of the allowable pressures in the force main. Therefore, the peak flows exceeded the flow capacity at the Poplin Road pump station.

There is available capacity for the Sanctuary at Southgate Phase 2 development to connect to the 12-inch sewer. No SSOs were predicted in the 12-inch or 8-inch downstream gravity systems. However, the current firm pumping capacity of the Fieldstone and Poplin Road pump stations are inadequate to handle the additional wet weather flows from the new development.

GRAVITY SEWERS

The graphs in Figure 3 and Figure 4 below show the flow and depth in the sewer downstream of the new connection where the 12-inch sewer receives flow from this project and other tributary permitted project flows tributary to the Fieldstone pump station. The total flow at MH-14726 includes the obligated flows, as well as flows from the Sanctuary at Southgate Phase 2 development flows. Depth was not observed in the model to exceed the crown of pipe at this point in the collection system. Flow at this point prior to the development flows being added to



the model was 0.379 mgd. This increased to 0.624 mgd after Sanctuary at Southgate Phase 2 flows were added.

Figure 3 Peak Flow at MH-14726



Figure 4 Peak Depth at MH-14726

The graphs in Figure 5 and Figure 6 below show the flow and depth in the sewer downstream of the new connection where the 8-inch sewer receives discharge from the Fieldstone pump station. The total flow at MH-6336 includes flows from Fieldstone, and the developments previously indicated within that service area. Depth was not observed in the model to exceed the crown of pipe at this point in the collection system. The peak flow in the pipe at this point before the Sanctuary at Southgate Phase 2 development was added was 0.44 mgd. With the development online, the peak flow increased to 0.69 mgd.



Figure 5 Peak Wet Weather Flow at MH-6336



Figure 6 Peak Depth at MH-6336

Sewer capacity evaluations for the alternative flow route, sending project flows to the Porter Ridge pump station service area, were very similar to the results of the evaluation for the original connection point. The effect of moving the development's proposed flows to a more downstream point essentially return flows to predevelopment conditions upstream of the Porter Ridge pump station discharge manhole. There were no capacity limitations in the modeled 12-inch sewer in the original flow route, or in in the alternative flow route. This alternate flow route has no effect on the model results obtained at the Fieldstone or Poplin Road pump stations downstream. The capacity of the Porter Ridge pump station was not evaluated in this analysis, but it is recommended that the station's average flow, obligated flows, and firm capacity be evaluated in order to further assess the impact of this development on that station.

FIELDSTONE PUMP STATION AND FORCE MAIN

Table 2 summarizes the dry weather flows at the Fieldstone pump station. The station was evaluated for capacity based on the most recent drawdown test data shown in Table 3 and the existing flows in the model. The criteria that would trigger an improvement for a pump station is the pump station not having firm capacity to pump the flows during a 1-year design storm. The firm capacity of the Fieldstone Pump Stations is 0.44 mgd. The average flows to the pump station are approximately 0.21 mgd; therefore, there is approximately 0.23 mgd of available capacity at the pump station. This project's peak flows would exceed the allocation capacity of the station. The modeled peak flow to the Fieldstone pump station after the Sanctuary at Southgate development's flows come online exceed the station's firm capacity of 0.44 mgd. For these two reasons, there is not enough available capacity for the new development's flows.

Table 2 Fieldstone Pump Station Dry Weather Flows

Average Flow	Obligated Flow	Total Flow
(MGD)	(MGD)	(MGD)
0.09	0.12	0.21

Table 3 Fieldstone Pump Station Capacity

Fieldstone Pump Station			
Drawdown Test Date	Pump 1 Drawdown (MGD)	Pump 2 Drawdown (MGD)	Firm Capacity (MGD)
4/9/2020	0.44	0.45	0.44

POPLIN ROAD PUMP STATION AND FORCE MAIN

UCW provided draw down tests that approximated the Poplin Road Pump Station firm capacity at 4.0 mgd, however, as noted in the *Poplin Road Pump Station Alternatives Analysis* technical memo, the force main flow is limited because the allowable pressures of the force main are below the pressures caused by the firm capacity. Therefore, the flows were limited to 3.64 mgd. Table 4 summarizes the dry weather flows to the Poplin Road pump station. The model was run with the force main capacity limitation. and the existing flows into the Poplin Road Pump Station were estimated to be 4.07 mgd, which exceeds the wet weather capacity at the pump station. It should be noted that there is a planned CIP project to provide wet weather storage for the Poplin Road Pump Station by building a 3.0 mgd equalization basin for the wet weather flows. Once this project is implemented the capacity at the Poplin Road Pump Station can be reevaluated. This project is scheduled to be completed in the third quarter of 2023.

Table 4 Poplin Road Pump Station Dry Weather Flows

Average Flow	Obligated Flow	Total Flow
(MGD)	(MGD)	(MGD)
1.04	0.32	1.36

RECOMMENDATION

Both the 12-inch and 8-inch gravity sewers associated with the development flows evaluated in this analysis are not predicted to surcharge under a 1-year storm event. The alternate flow path for this development has little effect on the analysis in terms of capacity based on the modeling results but requires the construction of off-site gravity sewer conveying flows to the Porter Ridge pump station service area. The Porter Ridge pump station capacity needs to be evaluated if the alternate route is further considered. The allocation and firm capacities of the Fieldstone pump station are exceeded with the addition of this project's proposed peak flows. It is not recommended that the 0.44 mgd firm capacity of the station be exceeded. Approval of the development flows connecting to the UCW collection system cannot be granted for this reason. Furthermore, the allocation and firm capacities of the Poplin Road pump station are exceeded with the addition of this project's proposed peak flows. Approval for this development is dependent on completion of the CIP improvement project that will install adequate flow equalization at the Poplin Road Pump Station. Once an equalization tank is installed, the storage volume will be sufficient to prevent backup in the gravity system upstream of the Poplin Rd Pump Station. It should be noted that the Poplin Road Pump Station is pumping at full capacity for extended periods of time to empty the wet weather equalization tank and the 24-inch gravity sewer downstream of the force main discharge location is at full capacity. The 3.0 mgd Poplin Road equalization basin project is expected to be completed in the third guarter of 2023. Until this project is completed, it is not recommended that the 3.64 mgd operational capacity of the station be exceeded.

The Twelve Mile Creek WRF has a rated capacity of 7.5 MGD. North Carolina law 15A NCAC 02T.0118, often referred to as the 80/90 rule, states that prior to exceeding 80% of the wastewater treatment system's permitted hydraulic capacity based on average flow of the last calendar year, an evaluation on meeting future wastewater needs must be submitted to the State. Additionally, at 90% plant capacity, final plans and specifications for expansion must be submitted and approved. Based on the 80/90 Rule, UC should be ready to submit an evaluation of their future treatment needs and outline plans going forward by the time the average annual flow exceeds 80% of the permitted treatment capacity (6 MGD). Current flows are approaching the 80% mark and UC should be prepared to submit an evaluation in the near future.

Very truly yours, **BLACK & VEATCH INTERNATIONAL COMPANY** CAROLIN 038316 038316 007 C. THOMPSOT Scot Thompson **Project Manager** NPH John Shutak, UCW cc: Jeff Coggins, BV Katy Weidner BV



24 August 2023

Union County Water 500 N. Main Street, Suite 500 Monroe, NC 28112 Wastewater Collection System Analysis Sanctuary at Southgate Phase 2 Revised Black & Veatch Project 175886.8063

Attention: Crystal Outlaw Panico, PE

BACKGROUND

Union County Water (UCW) has requested that Black & Veatch update hydraulic analyses for the proposed Sanctuary at Southgate development utilizing UCW's collection system hydraulic model. Previous hydraulic analyses, reported in the recent April 2023 technical memo contain model results for project wastewater flows conveyed through the Fieldstone and Porter Ridge pump stations. This analysis is intended to evaluate the impacts along two alternative sewer routes: Sedgewick Rd sewer and Potomac Rd sewer. The proposed Sanctuary at Southgate Phase 2 development would be tributary to the Poplin Road pump station, which pumps receiving flows into the Twelve Mile Creek Basin.

DEVELOPMENT OVERVIEW

Based on the Utility Sketch Plan document prepared by BGE, Inc, dated July 7, 2022 the site will consist of 75 single family homes, 240 three-bedroom multi-family units, one clubhouse and pool, 24,500 SF of commercial development, a 200 seat restaurant, and an emergency response building. The development is located south of the intersection of Poplin Road and North Rocky River Road. The site is ±72 acres and Figure 1 shows a plan view of the proposed development.



Figure 1 Development Overview

ESTIMATED DEVELOPMENT WASTEWATER FLOWS

The developer's sketch included an estimate of total average daily flow of 97,870 gpd for the development. Table 1 summarizes the development's wastewater flows. In addition to the average daily flow estimates provided by the developer, the peak wet weather flows were estimated using a peaking factor of 3 for single family homes and a peaking factor of 2.5 for multi-family homes and commercial. The peak flows incorporate an infiltration and inflow (I/I) flow component for the proposed development and is in line with the peaking factors observed in the UCW 2011 Comprehensive Master Plan I/I estimates for new developments.

Flow Source	Number of Units/Size	Unit	Unit Rates	Average Daily Flow (gpd)	Peak Wet Weather Flow (gpd)		
Single Family Residential Units	75	Units	280	21,000	63,000		
Multi-Family Units	720	Bedrooms	70	50,400	126,000		
Pool	1	Unit	1,670	1,670	4,175		
Clubhouse	10	Fixtures	250	2,500	6,250		
Commercial / Retail		-	-	22,300*	55,750		
Total 97,870 255,175							
*Total commercial / retail calcs on project utility plans page U1-0 (total of 22,300 gpd) do not match page U1-1 calculations (total of 24,300 gpd)							

Table 1 Sanctuary at Southgate Phase 2 Development Wastewater Flows Summary

DEVELOPMENT ANALYSIS

Figure 2 is a map of the project location and contains a red and blue dashed lines indicating the potential wastewater flow paths for the development. The development contains an on-site pump station on the southeast portion of the site, according to site utility plans. The pump station would pump flows from Phase 2 of the development and discharge to the northwest across Poplin Rd into one of two possible gravity sewers along either Sedgewick Rd or Potomac Rd. From either discharge location, these gravity sewers convey flow approximately 2,000 feet to the Poplin Road Pump Station.



Figure 2 Development Location and Flow Paths

An initial model run was performed to simulate existing 2022 conditions within the Twelve Mile Creek model network under the 2022 Comprehensive Master Plan design storm event, a 1- year SCS Type II storm with a 24-hour duration. The 2022 model run was then adjusted to include the new Sanctuary at Southgate Phase 2 development. The impact to the collection system was compared to the predevelopment conditions including the receiving gravity sewer and the downstream system.

DEVELOPMENT RESULTS

The Sanctuary at Southgate Phase 2 pump station would pump flows from the project site to the northwest across Poplin Rd into either 8-inch sewer along Sedgewick Rd, or into 8-inch sewer along Potomac Rd. After being discharged to one of these 8-inch sewers, wastewater will flow downstream by gravity to the existing 36-inch sewer leading into the Poplin Rd pump station. The 2022 model was updated to show the new development flows going to the indicated connection point. Model flows were compared against the UCW criteria for

improvements in the wastewater collection system. The criteria that would trigger an improvement in the UCW gravity sewers is 50% of the MH depth surcharged above the crown of the pipe during a 1-year design storm.

The model predicts there will be no surcharge in pipes downstream of the development, and the addition of the Sanctuary at Southgate Phase 2 development flow does not increase the peak flows significantly. The peak flow to the Poplin Road pump station is 4.07 mgd; however, the firm pumping capacity of the Poplin Road pump station is limited to 3.64 mgd because of the allowable pressures in the force main. Therefore, the peak flows exceeded the flow capacity at the Poplin Road pump station.

There is available capacity for the Sanctuary at Southgate Phase 2 development to connect to the 8-inch sewers on both Sedgewick Rd and Potomac Rd. Surcharging in these sewers did not exceed the crown of the pipe and no SSOs were predicted in the downstream gravity systems. However, the current firm pumping capacity of the Poplin Road pump station is inadequate to handle the additional wet weather flows from the new development.

GRAVITY SEWERS

The graphs in Figures 3 through Figure 6 below show the flow and depth in the sewer downstream of the new connection at locations on both Sedgewick Rd and Potomac Rd where manhole depth is the least, meaning surcharging due to wet weather flow would be of most concern. The total flow at MH-6276 (Sedgewick route) and MH-6281 (Potomac route) includes the obligated flows, as well as flows from the Sanctuary at Southgate Phase 2 development flows. Depth was not observed in the model to exceed the crown of pipe at these points in the collection system. Flow at these points prior to the development flows being added to the model were 0.0141 mgd and 0.0013 mgd, and increased to 0.313 mgd and 0.304 mgd, respectively, after Sanctuary at Southgate Phase 2 flows were added.



Figure 3 Peak Flow at MH-6276 (Sedgewick Route)



Figure 4 Peak Depth at MH-6276 (Sedgewick Route)



Figure 5 Peak Wet Weather Flow at MH-6281 (Potomac Route)



Figure 6 Peak Depth at MH-6281 (Potomac Route)

POPLIN ROAD PUMP STATION AND FORCE MAIN

UCW provided draw down tests that approximated the Poplin Road Pump Station firm capacity at 4.0 mgd, however, as noted in the *Poplin Road Pump Station Alternatives Analysis* technical memo, the force main flow is limited because the allowable pressures of the force main are below the pressures caused by the firm capacity. Therefore, the flows were limited to 3.64 mgd. Table 2 summarizes the dry weather flows to the Poplin Road pump station. The model was run with the force main capacity limitation. and the existing flows into the Poplin Road Pump Station were estimated to be 4.07 mgd, which exceeds the wet weather capacity at the pump station. It should be noted that there is an ongoing CIP project to provide wet weather storage for the Poplin Road Pump Station by building a 4.0 MG equalization basin for wet weather flows. Once this project is implemented the capacity at the Poplin Road Pump Station can be reevaluated. This project is scheduled to be completed in the third quarter of 2023.

Table 2 Po	plin Road	Pump	Station	Drv	Weather	Flows
	philittoud	i unip	otation	~,	ricutifer	10110

Average Flow	Obligated Flow	Total Flow
(MGD)	(MGD)	(MGD)
1.04	0.32	1.36

RECOMMENDATION

Both 8-inch gravity sewer discharge alternatives evaluated in this analysis are not predicted to surcharge under a 1-year storm event. Either location is viable from a capacity standpoint. The allocation and firm capacities of the Poplin Road pump station are exceeded with the addition

of this project's proposed peak flows. Approval for this development is dependent on completion of the CIP improvement project that will provide flow equalization at the Poplin Road Pump Station. At that point, the storage volume will be sufficient to prevent backup in the gravity system upstream of the Poplin Road Pump Station. It should be noted that the model runs project the Poplin Road Pump Station to be pumping at full capacity for extended periods of time to empty the equalization basin; meanwhile, the 24-inch gravity sewer downstream of the force main discharge location is at full capacity. Until the Poplin Road Pump Station EQ Basin project is completed, it is not recommended that the 3.64 mgd operational capacity of the station be exceeded.

The Twelve Mile Creek WRF has a rated capacity of 7.5 MGD. North Carolina law 15A NCAC 02T.0118, often referred to as the 80/90 rule, states that prior to exceeding 80% of the wastewater treatment system's permitted hydraulic capacity based on average flow of the last calendar year, an evaluation on meeting future wastewater needs must be submitted to the State. Additionally, at 90% plant capacity, final plans and specifications for expansion must be submitted and approved. Based on the 80/90 Rule, UC should be ready to submit an evaluation of their future treatment needs and outline plans going forward by the time the average annual flow exceeds 80% of the permitted treatment capacity (6 MGD). Current flows are approaching the 80% mark and UC should be prepared to submit an evaluation in the near future.

Very truly yours, **BLACK & VEATCH INTERNATIONAL COMPANY** anninn CARO Scot Thompson **Project Manager** NPH John Shutak, UCW cc: Jeff Coggins, BV

Katy Weidner BV Nathan Hampton BV

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APPENDIX 7 - PUMP STATION ALTERNATIVES

ALTERNATIVE 1



Figure 2 Development Location and Flow Paths

Note: Alternative 1 is defined in Black & Veatch's Phase 2 Wastewater Collection System Analysis, dated 8/24/2023, and Figure 2 is included in the report (See Appendix 6).



Note: The Alternative 2 graphic was developed by Black & Veatch and included in the Sanctuary at Southgate Gravity Alternative Calculations, dated 11/21/2023 (See Appendix 8).

ALTERNATIVE 2



Union County Water - Sanctuary at Southgate Gravity Calculations

Known Information and Assumptions:

- Sanctuary at Southgate is located at Poplin Rd and Rocky River Rd.
- The nearest Union County infrastructure downstream of the development is the Porter Ridge Pump Station
- Flow Calculations
 - Flow for the Sanctuary at Southgate Phase 2 project were outlined in the received sketch plan
- Slope assumptions using the approximate ground slope from Digital Elevation model:
 - The gravity sewer from the development location to the South Fork of Crooked Creek would be 4,900 ft. The elevation change is 24 ft. The ground slope is approximately 0.49%.
 - The sewer along the South Fork of Crooked Creek is 2200 ft and would need to be installed at minimum slope (0.4%).
- Length of sewer: 7,100 ft
- Manning's n=0.013
Estimated Flow in Sewer

	Avg Flow (gpd)	Wet Weather Flow (gpd)
Sanctuary at Southgate Phase II	97,870	255,175

0.255 mgd = 0.395 cfs

Pipe Size Calculations

$$d = \left(\frac{(Q*n)}{(0.46*\sqrt{S})}\right)^{3/8} = \left(\frac{(0.395*0.013)}{(0.46*\sqrt{0.004})}\right)^{3/8} = 0.50 \ ft = 6 \ in$$

Since the minimum gravity size is an 8=inch, a pipe diameter of **8 inches** is recommended for the gravity sewer.

Estimated Flow at Porter Ridge Pump Station

Porter Ridge Existing Firm Capacity = 180 gpm = 0.259 mgd

School WW Peaking Factor = 2.5

- Porter Ridge HS, assumed 1800 students, 100 faculty
 - o 15 gal/student
 - o **27,000 gpd**
- Porter Ridge MS, assumed 1300 students, 70 faculty
 - o 15 gal/student
 - o **19,500 gpd**
- Porter Ridge ES, assumed 600 students, 40 faculty
 - o 12 gal/student
 - o 7,200 gpd

	Avg Flow (gpd)	Wet Weather Flow (gpd)
Current Porter Ridge Flows (schools)	53,700	134,250
Sanctuary at Southgate Phase II	97,870	255,175
Total		389,425

0.389 mgd = 0.602 cfs = 270.4 gpm

<u>Recommendation</u>: Replace the Porter Ridge PS pumps with 275 gpm pumps at 105 ft of head. This larger size would not provide for any additional capacity for future upstream connections. The 6-inch force main is adequately sized. The velocity in the 6-inch force main would be about 3 fps at a flow of 270 gpm.

<u>Fieldstone Pumps</u>: The 2 pumps would need to be swapped for new pumps at a design point of 490 gpm at approximately 102 ft of head. This would be enough flow for the current obligated flows and the

Sanctuary at Southgate development. This would not allow for any capacity for future upstream connections.

<u>Fieldstone Force Main</u>: The 6-inch force main would be fine. At 490 gpm, the velocity in the force main is 5.5 fps, and the discharge pressure is reasonable.

<u>Fieldstone Wet Well</u>: The new pump would pump almost twice as much flow as the existing pumps. We would need to review the drawings to determine if improvements were needed to limit the number of on/off cycles.

Final List of Projects:

- 7,100 ft of 8-inch gravity sewer from the development site to the Porter Ridge PS
- 2 new pumps at the Porter Ridge PS (275 gpm at 105 feet of head)
- 2 new pumps at the Fieldstone PS (490 gpm at 102 feet of head)
- The pump sizing at each station is increasing by 30-50%. Wet Well Improvements may be required depending on size of new pumps and existing wet well, both ensure to fit the pumps themselves fit in the pump slots and that the size provides adequate volume to limit the number of on/off cycles. The sizing of the existing electrical systems and the generator should also be assessed to determine whether they can support the larger pumps.

APPENDIX 9 - NEW SANCTUARY AT SOUTHGATE PHASE II PUMP STATION CALCULATIONS



199

200.00

1.00

Pump Station Sizing and Cycles

Proj	ect Name:	Sanctuary at Southgate PS		Designed By:	APG	Date:	12/20/2024	
Proj	ect Location:	UCPW in Indian Trail			Checked By:		Date:	
BGE	Project #:	7734-16		Revised By:			LMK	
Wo+	Wall Flowatio	n c						
wei	. well Elevatio	ns ound Elev –	608.00		High Lovel /	Varm Elov –	505 00	
	Gi Sower I	nvert Flev -	596.00		l ag Pum	$n \cap F = 0$	594.00	
Fc	Jewei I Arce Main Discl		602.22		Lag Full	n On Elev -	502.00	
FC	Top of I	Dumn Flov –	590.00		Leau Full Pumr	ns Off Floy –	590.50	
	Pump Su	ction Elev -	587.50			Varm Flev -	590.00	
	Wet Well	Sumn Elev =	587.30		LOW LEVELP		550.00	
	wet wen.		507.25					
Wet	: Well Dimensi	ons						
	Wet Well	Diameter =	6.00	Wet V	Vell Active Stora	age Depth =	2.50	
	Wet Well Stora	ge per Foot =	28.3 cf/ft	Wet We	ell Active Storag	e Volume =	528.7 gal.	
	Wet Well Stora	ge per Foot =	211.5 gal./ft					
_								
Pum	np Station Cycl	es						
1.	Cycles at Begi	nning of Life						
	Pum	p Rate at Beg	ginning of Life =	225.00 gpm	Cy	cle Time T =	11.1 min.	
		Active S	torage Volume =	528.7 gal.	Cycles	8 Per Hour =	5.38	
		Desi	gn Daily Flow =	68.0 gpm				
	Inflow Rate	Pumn Rate	Net Flow Rate	Draw Down	Time to Fill	Cycle Time	Cycles Per	Volume
	(gnm)	(gnm)	Out (gpm)	Time (gnm)	(min)	(min)	Hour	Pumped
	1	225.00	224.00	2.36	528.73	531.09	0.11	531.09
	50	225.00	175.00	3.02	10.57	13.60	4 41	679.80
	67.97 gpm	225.00	157.03	3.37	7.78	11.15	5.38	757.57
	100	225.00	125.00	4 23	5.29	9.52	6 30	951 71
	150	225.00	75.00	7.05	3.52	10.57	5.67	1586.19
	177.20 gpm	225.00	47.80	11.06	2.98	14.05	4.27	2489.05
	224	225.00	1.00	528.73	2.36	531.09	0.11	118964.26
2.	Cycles at End	of Life						
		Pump Rate	at End of Life =	200.00 gpm	Су	cle Time T =	11.8 min.	
		Active S	torage Volume =	528.7 gal.	Cycles	8 Per Hour =	5.09	
		Desi	gn Daily Flow =	68.0 gpm				
	Inflow Rate	Pump Rate	Net Flow Rate	Draw Down	Time to Fill	Cycle Time	Cycles Per	
	(gpm)	(gpm)	Out (gpm)	Time (gpm)	(min)	(min)	Hour	
	1	200.00	199.00	2.66	528.73	531.39	0.11	
	50	200.00	150.00	3.52	10.57	14.10	4.26	
	67.97 gpm	200.00	132.03	4.00	7.78	11.78	5.09	
	100	200.00	100.00	5.29	5.29	10.57	5.67	
	150	200.00	50.00	10.57	3.52	14.10	4.26	
	177.20 gpm	200.00	22.80	23.19	2.98	26.18	2.29	

528.73

2.66

531.39

0.11



Pump Station Major Losses

	2024
Project Location: UCPW in Indian Trail Checked By: Date:	
BGE Project #: 7734-16 LMK Date:	

Pump Station Major Losses

1. Static Head

Force Main Max CL Elevation =	630.00
Pump Suction Elevation =	587.50
Static Head =	42.50 ft.

2. Suction Head

Suction Head =	-3.00 ft.
Pump Suction Elev =	587.50
Pumps Off Elev =	590.50

3. Friction Head

Pipe Size (in.)	Pipe Material	Pipe Length (ft.)	Inside Diameter (in.)	B.O.L. Pump Rate (gpm)	B.O.L. Hazen Williams Coefficient	B.O.L. Velocity (ft/sec)	E.O.L. Pump Rate (gpm)	E.O.L. Hazen Williams Coefficient	E.O.L. Velocity (ft/sec)
4	DI	40	4.18	225	125	5.26	200	100	4.67
4	PVC-SDR 18	0	4.23	225	140	5.14	200	120	4.56
6	DI	0	6.40	225	125	2.24	200	100	1.99
6	PVC-SDR 18	5460	6.09	225	140	2.48	200	120	2.20
8	DI	0	8.55	225	125	1.26	200	100	1.12
8	PVC-SDR 18	0	7.98	225	140	1.44	200	120	1.28

Beginning of Life Friction Head = **21.87 ft.**

End of Life Friction Head = 23.56 ft.



Pump Station Minor Losses and Total Head Losses

Project Name:	Sanctuary at Southgate PS	Designed By:	APG	Date:	12/20/2023
Project Location:	UCPW in Indian Trail	Checked By:		Date:	
BGE Project #:	7734-16	Revised By:		Date:	

Pump Station Minor Losses

1. Fitting Losses

Pine Size	Fitting	Friction Loss	B.O.L.	BOL Head	E.O.L.	E.O.L.
(in)	Description	Coefficient	Velocity	Loss (ft)	Velocity	Head Loss
(111.)	Description	(k)	(ft/sec)	2033 (11.)	(ft/sec)	(ft.)
4	Std. 90° Bend	0.51	5.26	0.22	4.67	0.17
4	Std. 90° Bend	0.51	5.26	0.22	4.67	0.17
4	Plug Valve	0.31	5.26	0.13	4.67	0.11
4	Swing Check	0.90				
4	Valve	0.90	5.26	0.39	4.67	0.31
4	Tee-Branch	1.02	5.26	0.44	4.67	0.35
6	Tee-Through	0.90	2.24	0.07	1.99	0.06
6	4x6 Increase	0.28	2.24	0.02	1.99	0.02
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	45° Bend	0.24	2.24	0.02	1.99	0.01
6	22.5° Bend	0.12	2.24	0.01	1.99	0.01
6	22.5° Bend	0.12	2.24	0.01	1.99	0.01
6	Pipe Exit	1.00	2.24	0.08	1.99	0.06

Beginning of Life Friction Head =	1.94
End of Life Friction Head =	1.53

Pump Station Total Head Losses

1. Beginning of Life Total Head Losses

Static Head =	42.50
Suction Head =	-3.00
Friction Head Losses =	21.87
Fitting Head Losses =	1.94
Total System Head =	63.31 ft.

2.	End of Life Total Head Losses
	Charles Hand

Total System Head =	64.60 ft.
Fitting Head Losses =	1.53
Friction Head Losses =	23.56
Suction Head =	-3.00
Static Head =	42.50



Pump Station System Table

Project Name:	Sanctuary at Southgate PS	Designed By:	APG	Date:	12/20/2023
Project Location:	UCPW in Indian Trail	Checked By:		Date:	
BGE Project #:	7734-16	Revised By:		Date:	

Pump Station Minor Losses

1. Fitting Losses

Pump Rate	Avg.	Fitting	B.O.L.	B.O.L. Total	E.O.L.	E.O.L. Total	Head from NP
rump Kate	Velocity	Head Loss	Friction Head	System	Friction Head	System	2171 Dump Curvo
(ghu)	(ft/sec)	(ft.)	Loss (ft.)	Head (ft.)	Loss (ft.)	Head (ft.)	SI/I Pullip Curve
0	0.00	0.00	0.00	39.50	0.00	39.50	183.5
50	0.55	0.08	1.31	40.89	1.74	41.32	
100	1.11	0.33	4.71	44.54	6.27	46.10	175.5
150	1.66	0.75	9.97	50.22	13.28	53.52	
200	2.21	1.33	16.98	57.81	22.60	63.44	167.5
250	2.77	2.08	25.66	67.24	34.16	75.74	
300	3.32	2.99	35.96	78.45	47.86	90.35	161.0
350	3.87	4.07	47.82	91.40	63.65	107.23	
400	4.42	5.32	61.22	106.04	81.49	126.31	154.0
450	4.98	6.74	76.13	122.36	101.33	147.57	
500	5.53	8.32	92.51	140.33	123.14	170.95	147.0
550	6.08	10.06	110.35	159.91	146.88	196.44	
600	6.64	11.98	129.62	181.10	172.53	224.01	142.5
650	7.19	14.05	150.31	203.86	200.07	253.63	
700	7.74	16.30	172.40	228.20	229.47	285.27	136.0



Anti-Floatation Sizing

Project Name:	Sanctuary at	Southgate PS	Designed By: APG	Date: 12/20/2023	
Project Location:	UCPW in Indi	an Trail	Checked By: APG	Date: 12/20/2023	
BGE Project #:	7734-16		Revised By:		
Wet Well Dimensions			Unit Weights		
Тор	of Wet Well Elev =	609.00	Unit Weight of Concrete =	150 lbs./cu. ft.	
Fin	ished Grade Elev =	608.00	Unit Weight of Saturated Soil =	105 lbs./cu. ft.	
We	t Well Sump Elev =	587.25	Unit Weight of Water =	62.4 lbs./cu. ft.	
W	et Well Diameter =	6.00 ft.	-		
Тс	op Slab Thickness =	1.00 ft.	Wet Well Weights		
	Wall Thickness =	0.67 ft.	Weight of Top Slab =	6,347.07 lbs.	
	Base Thickness =	1.00 ft.	Weight of Wet Well =	43,697.83 lbs.	
Antifloatatio	on Base Diameter =	14.00 ft.	Weight of Base =	6,347.07 lbs.	
Antifloatatio	n Base Thickness =	2.00 ft.	Weight. of Antifloatation Base =	33,487.27 lbs.	
Depth of Wet Well embedded	d into Antifloatation			89,879.24 lbs.	
	Base =	2.00 ft.			
Vo	ume of Top Slab =	42.31 cu. ft.	Soil Weight Above Antifloata	tion Base	
Vol	ume of Wet Well =	878.01 cu. ft.	Volume of Soil =	2204.58 cu. ft.	
	Volume of Base =	42.31 cu. ft.	Weight of Soil =	231,480.77 lbs.	
Vol. of Ar	ntifloatation Base =	223.25 cu. ft.	<u> </u>	· · · ·	
Total	Vol. of Wet Well =	1185.89 cu. ft.	Anti-Buoyant Force of Wet Well =	146,404.53 lbs.	
			•		
Buoyant Fo	orce of Wet Well =	73,999.37 lbs.	Factor of Safety =	1.98	FS Should be a

APPENDIX 10 - NEW SANCTUARY AT SOUTHGATE PHASE II PUMP STATION - FLYGT NP 3127 PUMP



Phases

Number of poles

Rated voltage

3~

4

460 V

90.3 %

Technical specification

Motor - General

Motor number N3127.920 21-12-4AS-W IE3 11hp ATEX approved No

Frequency

60 Hz

Version code 920

Motor - Technical

Power factor - 1/1 Load 0.90

Power factor - 3/4 Load 0.87

Power factor - 1/2 Load 0.79

92.1 % Motor efficiency - 3/4 Load 92.0 % Motor efficiency - 1/2 Load

Motor efficiency - 1/1 Load

Total moment of inertia 1.25 lb ft²

Rated speed

Rated current

Insulation class

. 1800 rpm

12 A

н

Starting current, direct starting 87 A

Starting current, star-delta 29 A

Project Block

Xylect-20620200

Created by Dan Joyce 9/16/2024 Last update Created on

9/16/2024



Rated power 11 hp Stator variant

Type of Duty S1

60

30

Starts per hour max.



Data version 8/29/2024 13:07 A8P8



Duty Analysis







a **xylem** brand



Usergroup(s) Xylem:USA-INT



VFD Analysis





VFD Analysis



Dimensional drawing





Usergroup(s) Xylem:USA-INT

APPENDIX 11 - ALTERNATIVE 1 LIFE CYCLE COST ANALYSIS

Life Cycle Cost Analysis Sanctuary at Southgate Phase II Development Alternative 1 - On-Site Pump Station with Gravity Sewer Connection at Annandale Subdivision						
Innuts and Assumptions						
Planning Period	20	Years			O&M Costs (% of Capital for Pump Stations)	3%
Discount Rate	1.55%	rouro			10-year Items (% of Total for Pump Stations)	5%
Inflation	3.20%				20-year Items (% of Total for Pump Stations)	60%
					50-year Items (% of Total for Pump Stations)	35%
Initial Capitol Investment						
Item	Quantity	UOM	Cost Per Unit	Cost		
6" PVC Sanitary Sewer Force Main	5460	LF	\$60	\$327,600		
New Sanctuary at Southgate Phase II Pump Station	1	LS	\$963,000	\$963,000		
			Total	\$1,290,600	J	
Amount Oceante						
Annual Costs	* *					
	\$0.08	KWH				
Flygt NP 3127 HT 3~ 488	44.45					
Pump On Time Per Cycle (min)	11.15					
Pump Cycles Per Hour	5.38					
Flygt NP 3153 HT 3~ 466 Pump Horsepower	11					
Ave Daily Flow Rate (GPM)	68					
US MG / Year	35.73					
Pump Spec Energy (kWh/US MG)	408					
Yearly Cost of Electricity	\$1,166.33					
Yearly Cost of Pump Station O&M	\$38,718.00					
Total Yearly Costs at Year 0	\$39,884.33					
Total Annual Costs NPV	\$919,441.58					
Life-Cycle Replacement Costs						
Cost 10-year Items at Year 0	\$64 530 00					
Cost 10 year Items at Year 10	\$88 421 65					
NPV of 10-Year Itoms at Year 10	\$75 815 7 <i>1</i>					
Cost 10 year Itoms at Year 20	¢101 150 00					
NDV of 10 Year Items at Year 20	\$121,100.90					
Cast 20 Veer Items at Veer 0	\$09,075.25 \$774,260,00					
Cost 20-Year Items at Year 20	\$774,300.00					
Cost 20- real items at real 20	\$1,455,907.77					
NPV of 20-Year items at Year 20	\$1,068,903.02					
Total Life-Cycle Replacement Costs NPV	\$1,233,794.00					
Posidual Valuos						
Cast of 10 year Items at Year 20	¢101 150 00					
Cost of 20 year items at Year 20	⇒1∠1,100.98					
Cost of 20-year items at rear 20 Residual Value of 50 Veer Items at Veer 20	φ1,400,907.77					
Tetal Life Ovela Banlacement Basidual Value at Varia 20						
Total Life-Cycle Replacement Residual Value at Year 20	φ1,040,092.75 ¢1 257 024 70					
i otai kesidual value NPV	φ1,357,234.72					
Total Net Present Value	<mark>\$2,086,600.86</mark>					

APPENDIX 12 - PORTER RIDGE PUMP STATION CALCULATIONS



Pump Station Design Flows

Project Name:	Porter Ridge PS	Designed By: APG	Date: 12/20/2024
Project Location:	UCPW in Indian Trail	Checked By:	Date:
BGE Project #:	7734-16	Revised By:	Date:

Proposed Uses

2. Phase II

Use	Units	Quantity Per Unit		Population	Daily Flow Per	Daily Flow Per Use
Existing Schools			1 Lot	0.0		53,700 gpd
Sanctuary at Southgate Single Family			1 Person	0.0		21,000 gpd
Sanctuary at Southgate Multi-Family and Commercial			1 Person	0.0		76,870 gpd

people people

3.00

2.50

Design Flow

Proposed Flow =	151,570 gpd	Proposed Population =
Design Daily Flow =	151,570 gpd	Total Population =
Design Daily Flow =	105.26 gpm	Single Family
	100120 8011	Peaking Factor =
		Multi-Family and
		Commercial Peaking Factor =
Peak Hourly Flow =	389,425 gpd	
Peak Hourly Flow =	270.43 gpm	



Pump Station Sizing and Cycles

Proj	ect Name:	Porter Ridge PS			Designed By:	APG	Date:	12/20/2024
Proj	ect Location:	UCPW in Indian Trail			Checked By:		Date:	
BGE	Project #:	7734-16			Revised By:		LMK	
wet	: Well Elevation	ns 	500.00				577.50	
	Gr	ound Elev =	590.00		High Level A	Alarm Elev =	577.50	
Г	Sewer I		577.92		Lag Pur	ip On Elev =	570.75	
FC	Drce Main Disci	harge Elev =	585.33		Lead Pur	ip On Elev =	576.00	
		Pump Elev =	573.00		Pump	S Off Elev =	573.00	
	Pump Su	ction Elev =	570.50		LOW Level A	Alarm Elev =		
	wet went	sump Elev =	570.00					
Wet	Well Dimensi	ons						
	Wet Well	Diameter =	6.00	Wet V	Vell Active Stor	age Depth =	3.00	
	Wet Well Stora	ge per Foot =	28.3 cf/ft	Wet We	ell Active Storag	ge Volume =	634.5 gal.	
	Wet Well Stora	ge per Foot =	211.5 gal./ft		e e e e e e e e e e e e e e e e e e e			
Pum	np Station Cycl	es						
1.	Cycles at Begin	nning of Life						
	Pum	p Rate at Beg	ginning of Life =	300.00 gpm	Су	cle Time T =	9.3 min.	
		Active S	torage Volume =	634.5 gal.	Cycles	s Per Hour =	6.46	
	Design Daily Flow = <u>105.3 gpm</u>							
	Jufferry Data	Duran Data	Net Fleur Dete	Draw Dawn	Time to Fill	Cuele Time	Cualas Dar	Maluraa
	Inflow Rate	Pump Rate	Net Flow Rate	Draw Down	(min)	(min)	Cycles Per	Volume
	(gpm) 1			nme (gpm)	624.49	(11111)		Fumpeu
	1	300.00	299.00	2.12	12.60	15.00	0.09	761.27
	50	300.00	250.00	2.54	6.02	15.23	3.94	761.37
	105.20 gpm	300.00	194.74	3.20	0.05	9.29	0.40	977.40
	160	300.00	140.00	4.53	2.97	8.50	7.06	1359.59
	225	300.00	75.00	8.40	2.02	22.01	2.52	2537.90
	270.45 gpm	300.00	29.57	21.40	2.55	23.81	2.52	6437.90
	299	300.00	1.00	034.48	2.12	030.00	0.09	190342.82
2.	Cvcles at End	of Life						
		Pump Rate	at End of Life =	275.00 gpm	Cv	cle Time T =	9.8 min.	
		Active S	torage Volume =	634.5 gal.	Cycles	s Per Hour =	6.14	
		Desi	gn Daily Flow =	105.3 gpm	-,			
			5					
	Inflow Rate	Pump Rate	Net Flow Rate	Draw Down	Time to Fill	Cycle Time	Cycles Per	
	(gpm)	(gpm)	Out (gpm)	Time (gpm)	(min)	(min)	Hour	
	1	275.00	274.00	2.32	634.48	636.79	0.09	
	50	275.00	225.00	2.82	12.69	15.51	3.87	
	105.26 gpm	275.00	169.74	3.74	6.03	9.77	6.14	
	160	275.00	115.00	5.52	3.97	9.48	6.33	
	225	275.00	50.00	12.69	2.82	15.51	3.87	
	270.43 gpm	275.00	4.57	138.96	2.35	141.30	0.42	
	274	275.00	1.00	634.48	2.32	636.79	0.09	



Pump Station Major Losses

Project Name:	Porter Ridge PS	Designed By:	APG
Project Location:	UCPW in Indian Trail	Checked By:	
BGE Project #:	7734-16	LMK	

Date: 12/20/2024 Date: Date:

Pump Station Major Losses

1. Static Head

Force Main Max CL Elevation =	613.00
Pump Suction Elevation =	570.50
Static Head =	42.50 ft.

2. Suction Head

Suction Head =	-2.50 ft.
Pump Suction Elev =	570.50
Pumps Off Elev =	573.00

3. Friction Head

Pipe Size (in.)	Pipe Material	Pipe Length (ft.)	Inside Diameter (in.)	B.O.L. Pump Rate (gpm)	B.O.L. Hazen Williams Coefficient	B.O.L. Velocity (ft/sec)	E.O.L. Pump Rate (gpm)	E.O.L. Hazen Williams Coefficient	E.O.L. Velocity (ft/sec)
4	DI	0	4.18	300	125	7.01	275	100	6.43
4	PVC-SDR 18	0	4.23	300	140	6.85	275	120	6.28
6	DI	0	6.40	300	125	2.99	275	100	2.74
6	PVC-SDR 18	8000	6.09	300	140	3.30	275	120	3.03
8	DI	0	8.55	300	125	1.68	275	100	1.54
8	PVC-SDR 18	0	7.98	300	140	1.92	275	120	1.76

Beginning of Life Friction Head = **51.65 ft.**

End of Life Friction Head = 58.48 ft.



Pump Station Minor Losses and Total Head Losses

Project Name:	Porter Ridge PS	Designed By:	APG Date	: 12/20/2024
Project Location:	UCPW in Indian Trail	Checked By:	Date	:
BGE Project #:	7734-16	Revised By:	Date	:

Pump Station Minor Losses

1. Fitting Losses

Pipe Size	Fitting	Friction Loss Coefficient	B.O.L. Velocity	B.O.L. Head	E.O.L. Velocity	E.O.L. Head Loss
(in.)	Description	(k)	(ft/sec)	LOSS (IL.)	(ft/sec)	(ft.)
4	Std. 90° Bend	0.51	7.01	0.39	6.43	0.33
4	Std. 90° Bend	0.51	2.99	0.07	2.74	0.06
4	Plug Valve	0.31	2.99	0.04	2.74	0.04
4	Swing Check	0.90				
4	Valve	0.50	2.99	0.13	2.74	0.11
4	Tee-Branch	1.02	2.99	0.14	2.74	0.12
6	Tee-Through	0.90	2.99	0.13	2.74	0.11
6	4x6 Increase	0.28	2.99	0.04	2.74	0.03
6	45º Bend	0.24	2.99	0.03	2.74	0.03
6	45º Bend	0.24	2.99	0.03	2.74	0.03
6	45° Bend	0.24	2.99	0.03	2.74	0.03
6	45° Bend	0.24	2.99	0.03	2.74	0.03
6	45º Bend	0.24	2.99	0.03	2.74	0.03
6	45° Bend	0.24	2.99	0.03	2.74	0.03
6	45° Bend	0.24	2.99	0.03	2.74	0.03
6	45º Bend	0.24	2.99	0.03	2.74	0.03
6	45º Bend	0.24	2.99	0.03	2.74	0.03
6	45º Bend	0.24	2.99	0.03	2.74	0.03
6	45° Bend	0.24	2.99	0.03	2.74	0.03
6	45° Bend	0.24	2.99	0.03	2.74	0.03
6	45º Bend	0.24	2.99	0.03	2.74	0.03
6	45º Bend	0.24	2.99	0.03	2.74	0.03
6	45º Bend	0.24	2.99	0.03	2.74	0.03
6	45º Bend	0.24	2.99	0.03	2.74	0.03
6	45° Bend	0.24	2.99	0.03	2.74	0.03
6	45° Bend	0.24	2.99	0.03	2.74	0.03
6	45° Bend	0.24	2.99	0.03	2.74	0.03
6	22.5° Bend	0.12	2.99	0.02	2.74	0.01
6	22.5° Bend	0.12	2.99	0.02	2.74	0.01
6	Pipe Exit	1.00	2.99	0.14	2.74	0.12

Beginning of Life Friction Head = End of Life Friction Head =

d =	1.74
= b	1.46

Pump Station Total Head Losses

1. Beginning of Life Total Head Losses

Static Head =	42.50
Suction Head =	-2.50
Friction Head Losses =	51.65
Fitting Head Losses =	1.74
Total System Head =	93.39 ft.

2.	End of Life Total Head Losses	
	C 1 1 1	

Total System Head =	99.94 ft.
Fitting Head Losses =	1.46
Friction Head Losses =	58.48
Suction Head =	-2.50
Static Head =	42.50



Pump Station System Table

Project Name:	Porter Ridge PS	Designed By:	APG	Date: 12/20/2024
Project Location:	UCPW in Indian Trail	Checked By:		Date:
BGE Project #:	7734-16	Revised By:		Date:

Pump Station Minor Losses

1. Fitting Losses

Dump Pata	Avg.	Fitting	B.O.L.	B.O.L. Total	E.O.L.	E.O.L. Total	Head from
Pullip Rate	Velocity	Head Loss	Friction Head	System	Friction Head	System	NP 3171
(gpiii)	(ft/sec)	(ft.)	Loss (ft.)	Head (ft.)	Loss (ft.)	Head (ft.)	Pump Curve
0	0.00	0.00	0.00	40.00	0.00	40.00	183.5
50	0.55	0.08	1.88	41.96	2.50	42.58	
100	1.10	0.33	6.77	47.10	9.00	49.33	175.5
150	1.65	0.75	14.33	55.07	19.05	59.80	
200	2.20	1.33	24.39	65.72	32.44	73.77	167.5
250	2.75	2.08	36.86	78.94	49.02	91.10	
300	3.30	2.99	51.65	94.64	68.69	111.68	161.0
350	3.85	4.07	68.69	112.76	91.36	135.43	
400	4.40	5.32	87.94	133.26	116.96	162.28	154.0
450	4.96	6.74	109.35	156.08	145.43	192.17	
500	5.51	8.32	132.88	181.20	176.73	225.05	147.0
550	6.06	10.06	158.50	208.57	210.81	260.87	
600	6.61	11.98	186.19	238.16	247.63	299.60	142.5
650	7.16	14.05	215.90	269.96	287.15	341.20	
700	7.71	16.30	247.63	303.93	329.34	385.64	136.0



Anti-Floatation Sizing

Project Name: Project Location: BGE Project #:	Porter Ridge PS n: UCPW in Indian Trail 7734-16		Designed ByAPGChecked By:APGRevised By:0	Date: 12/20/2024 Date: 12/20/2024 LMK
Wet Well Dimens	ions		Unit Weights	
Top of Wet	Well Elev =	591.00	Unit Weight of Concrete =	150 lbs./cu. ft.
Finished (Grade Elev =	590.00	Unit Weight of Saturated Soil =	105 lbs./cu. ft.
Wet Well	Sump Elev =	570.00	Unit Weight of Water =	62.4 lbs./cu. ft.
Wet Well Diameter =		6.00 ft.		
Top Slab	Thickness =	1.00 ft.	Wet Well Weights	
Wall	Thickness =	0.67 ft.	Weight of Top Slab =	6,347.07 lbs.
Base Thickness =		1.00 ft.	Weight of Wet Well =	42,118.39 lbs.
Antifloatation Base	Diameter =	14.00 ft.	Weight of Base =	6,347.07 lbs.
Antifloatation Base	Thickness =	2.00 ft.	Weight. of Antifloatation Base =	33,487.27 lbs.
Depth of Wet We	ll embedded		Total Weight of Wet Well =	88,299.80 lbs.
into Antifloat	ation Base =	2.00 ft.	-	
Volume o	f Top Slab = $\frac{-}{2}$	42.31 cu. ft.	Soil Weight Above Antifle	oatation Base
Volume of	Wet Well =	846.28 cu. ft.	Volume of Soil =	2120.86 cu. ft.
Volume of Base =		42.31 cu. ft.	Weight of Soil =	222,690.36 lbs.
Vol. of Antifloatation Base =		223.25 cu. ft.	-	
Total Vol. of Wet Well =		1154.15 cu. ft.	Anti-Buoyant Force of Wet Well =	141,915.75 lbs.
Buoyant Force of	Wet Well =	72,019.09 lbs.	Factor of Safety =	1.97

APPENDIX 13 - FIELDSTONE PUMP STATION CALCULATIONS



Pump Station Design Flows

Project Name:	Fieldstone PS	Designed By: APG	Date:	12/20/2024
Project Location:	UCPW in Indian Trail	Checked By:	Date:	
BGE Project #:	7734-16	Revised By:	Date:	

Proposed Uses

2. Phase II

Use	Units	Quantity Per Unit	Population	Daily Flow Per Unit	Daily Flow Per Use
Existing Flows		1 Lot	0.0		90,000 gpd
Permitted Flows		1 Lot	0.0		122,180 gpd
Sanctuary at Southgate Single-Family		1 Person	0.0		21,000 gpd
Sanctuary at Southgate Multi-Family and Commercial		1 Person	0.0		76,870 gpd

Design Flow

Proposed Flow =	310,050 gpd	Proposed Population =	people
Design Daily Flow =	310,050 gpd	Total Population =	people
Design Daily Flow	215 21	Single Family	
Design Daily Flow =	215.31 gpm	Peaking Factor =	3.00
_		Multi-Family and	
		Commercial Peaking Factor =	2.50
Peak Hourly Flow =	785,625 gpd		
Peak Hourly Flow =	545.57 gpm		



450

545.57 gpm

559

560.00

560.00

560.00

110.00

14.43

1.00

Pump Station Sizing and Cycles

Proj	ect Name:	Fieldstone P	S		Designed By:	APG	Date:	12/20/2024
Proj	ect Location:	UCPW in Inc	lian Trail		Checked By:		Date:	
BGE	Project #:	7734-16			Revised By:		LMK	
\/.a+								
wet		ns ound Flow -	F01 93		Lligh Lough	Narma Flav -		
	G		591.82			Alarm Elev =	570.50	
Г	Sewer I		570.42		Lag Pull	ip On Elev =	570.00	
FC	Tara af r	harge Elev =	588.50		Lead Pur	ip On Elev =	569.00	
		Pump Elev =	500.50		Pump	S Off Elev =	566.50	
	Pump Su	ction Elev =	503.53		LOW LEVEL A	Alarm Elev =		
	wet went	sump Elev =	563.20					
Wet	Well Dimensi	ons						
	Wet Well	Diameter =	10.00	Wet V	Vell Active Stor	age Depth =	2.50	
	Wet Well Stora	ge per Foot =	78.5 cf/ft	Wet We	ell Active Storage	ge Volume =	1468.7 gal.	
	Wet Well Stora	ge per Foot =	587.5 gal./ft					
Pum	p Station Cvcl	es						
1.	Cvcles at Begin	nning of Life						
	, e	p Rate at Beg	ginning of Life =	600.00 gpm	Cv	cle Time T =	10.6 min.	
		Active S	torage Volume =	1468.7 gal.	Cycles	s Per Hour =	5.64	
		Desi	n Daily Flow =	215.3 gpm	-,			
-				01-				
	Inflow Rate	Pump Rate	Net Flow Rate	Draw Down	Time to Fill	Cycle Time	Cycles Per	Volume
	(gpm)	(gpm)	Out (gpm)	Time (gpm)	(min)	(min)	Hour	Pumped
	1	600.00	599.00	2.45	1468.69	1471.15	0.04	1471.15
	150	600.00	450.00	3.26	9.79	13.06	4.60	1958.26
	215.31 gpm	600.00	384.69	3.82	6.82	10.64	5.64	2290.73
	300	600.00	300.00	4.90	4.90	9.79	6.13	2937.39
	450	600.00	150.00	9.79	3.26	13.06	4.60	5874.78
	545.57 gpm	600.00	54.43	26.98	2.69	29.68	2.02	16190.78
	599	600.00	1.00	1468.69	2.45	1471.15	0.04	881216.74
2	Cualas et Fasi	- 6 1 :6-						
Ζ.	Cycles at End o	Dump Pata	at End of Life -	F60.00 mm	C.	olo Timo T –	11.1 min	
				1469 7 gol	Cycler		E1	
		Active S	n Daily Flow -	215 2 gpm	Cycles	SPELHOUL -	5.41	
		Desig	gri Dally Flow =	215.5 gpm				
	Inflow Rate	Pump Rate	Net Flow Rate	Draw Down	Time to Fill	Cycle Time	Cycles Per	
	(gpm)	(gpm)	Out (gpm)	Time (gpm)	(min)	(min)	Hour	
	1	560.00	559.00	2.63	1468.69	1471.32	0.04	
	150	560.00	410.00	3.58	9.79	13.37	4.49	
	215.31 gpm	560.00	344.69	4.26	6.82	11.08	5.41	
	300	560.00	260.00	5.65	4.90	10.54	5.69	

3.26

2.69

2.63

16.62

104.49

1471.32

3.61

0.57

0.04

13.35

101.80

1468.69



Pump Station Major Losses

Project Name:	Fieldstone PS	Designed By:	AP
Project Location:	UCPW in Indian Trail	Checked By:	
BGE Project #:	7734-16	LMK	

APG Date: 12/20/2024 Date: ______ Date: ______

Pump Station Major Losses

1. Static Head

Force Main Max CL Elevation =	625.00
Pump Suction Elevation =	563.53
Static Head =	61.47 ft.

2. Suction Head

Suction Head =	-2.97 ft.
Pump Suction Elev =	563.53
Pumps Off Elev =	566.50

3. Friction Head

Pipe Size (in.)	Pipe Material	Pipe Length (ft.)	Inside Diameter (in.)	B.O.L. Pump Rate (gpm)	B.O.L. Hazen Williams Coefficient	B.O.L. Velocity (ft/sec)	E.O.L. Pump Rate (gpm)	E.O.L. Hazen Williams Coefficient	E.O.L. Velocity (ft/sec)
4	DI	0	4.18	600	125	14.02	560	100	13.09
4	PVC-SDR 18	0	4.23	600	140	13.69	560	120	12.78
6	DI	0	6.40	600	125	5.98	560	100	5.58
6	PVC-SDR 18	4400	6.09	600	140	6.61	560	120	6.17
8	DI	0	8.55	600	125	3.35	560	100	3.13
8	PVC-SDR 18	0	7.98	600	140	3.85	560	120	3.59

Beginning of Life Friction Head = **102.40 ft.**

End of Life Friction Head = 119.88 ft.



Pump Station Minor Losses and Total Head Losses

Project Name:	Fieldstone PS	Designed By:	APG	Date: 12/20/2024
Project Location:	UCPW in Indian Trail	Checked By:		Date:
BGE Project #:	7734-16	Revised By:		Date:

Pump Station Minor Losses

1. Fitting Losses

Pipe Size (in.)	Fitting Description	Friction Loss Coefficient (k)	B.O.L. Velocity (ft/sec)	B.O.L. Head Loss (ft.)	E.O.L. Velocity (ft/sec)	E.O.L. Head Loss (ft.)
4	Std. 90° Bend	0.51	14.02	1.56	13.09	1.36
4	Std. 90° Bend	0.51	5.98	0.28	5.58	0.25
4	Plug Valve	0.31	5.98	0.17	5.58	0.15
4	Swing Check Valve	0.90	5.98	0.50	5.58	0.44
4	Tee-Branch	1.02	5.98	0.57	5.58	0.49
6	Tee-Through	0.90	5.98	0.50	5.58	0.44
6	4x6 Increase	0.28	5.98	0.16	5.58	0.14
6	45° Bend	0.24	5.98	0.13	5.58	0.12
6	45º Bend	0.24	5.98	0.13	5.58	0.12
6	45º Bend	0.24	5.98	0.13	5.58	0.12
6	45° Bend	0.24	5.98	0.13	5.58	0.12
6	45º Bend	0.24	5.98	0.13	5.58	0.12
6	45º Bend	0.24	5.98	0.13	5.58	0.12
6	45º Bend	0.24	5.98	0.13	5.58	0.12
6	45º Bend	0.24	5.98	0.13	5.58	0.12
6	45° Bend	0.24	5.98	0.13	5.58	0.12
6	45° Bend	0.24	5.98	0.13	5.58	0.12
6	45° Bend	0.24	5.98	0.13	5.58	0.12
6	22.5° Bend	0.12	5.98	0.07	5.58	0.06
6	22.5° Bend	0.12	5.98	0.07	5.58	0.06
6	Pipe Exit	1.00	5.98	0.56	5.58	0.48

Beginning of Life Friction Head =5.89End of Life Friction Head =5.13

Pump Station Total Head Losses

1. Beginning of Life Total Head Losses

Static Head = 61.47 Suction Head = -2.97 Friction Head Losses = 102.40 Fitting Head Losses = 5.89 Total System Head = **166.79 ft.**

2. End of Life Total Head Losses

Static Head =	61.47
Suction Head =	-2.97
Friction Head Losses =	119.88
Fitting Head Losses =	5.13
Total System Head =	183.51 ft.



Pump Station System Table

Project Name:	Fieldstone PS	Designed By:	APG	Date:	12/20/2024
Project Location:	UCPW in Indian Trail	Checked By:		Date:	
BGE Project #:	7734-16	Revised By:		Date:	

Pump Station Minor Losses

1. Fitting Losses

Rump Pato	Avg.	Fitting	B.O.L.	B.O.L. Total	E.O.L.	E.O.L. Total	Hood from NR
rump Kate	Velocity	Head Loss	Friction Head	System	Friction Head	System	2171 Dump Curvo
(ghu)	(ft/sec)	(ft.)	Loss (ft.)	Head (ft.)	Loss (ft.)	Head (ft.)	SI/I Pullip Curve
0	0.00	0.00	0.00	58.50	0.00	58.50	183.5
50	0.55	0.08	1.03	59.61	1.37	59.95	
100	1.10	0.32	3.72	62.54	4.95	63.77	175.5
150	1.65	0.72	7.88	67.10	10.48	69.70	
200	2.20	1.28	13.42	73.20	17.84	77.63	167.5
250	2.75	2.00	20.27	80.78	26.96	87.47	
300	3.30	2.88	28.41	89.79	37.78	99.16	161.0
350	3.85	3.92	37.78	100.20	50.25	112.67	
400	4.40	5.13	48.37	111.99	64.33	127.95	154.0
450	4.96	6.49	60.14	125.13	79.99	144.98	
500	5.51	8.01	73.08	139.59	97.20	163.71	147.0
550	6.06	9.69	87.18	155.37	115.95	184.14	
600	6.61	11.53	102.40	172.44	136.20	206.23	142.5
650	7.16	13.54	118.75	190.78	157.93	229.97	
700	7.71	15.70	136.20	210.39	181.14	255.34	136.0



Anti-Floatation Sizing

Project Name:	Fieldstone P	S	Designed By APG	Date: <u>12/20/2024</u>
Project Location:	UCPW in Inc	lian Trail	Checked By: APG	Date: 12/20/2024
BGE Project #:	7734-16		Revised By: 0	LMK
Wet Well Dimens	ions		Unit Weights	
Top of Wet	: Well Elev =	592.82	Unit Weight of Concrete =	150 lbs./cu. ft.
Finished (Grade Elev =	591.82	Unit Weight of Saturated Soil =	105 lbs./cu. ft.
Wet Well	Sump Elev =	563.20	Unit Weight of Water =	62.4 lbs./cu. ft.
Wet Well	Diameter =	10.00 ft.	-	
Top Slab	Thickness =	1.00 ft.	Wet Well Weights	
Wall	Thickness =	0.67 ft.	Weight of Top Slab =	15,149.81 lbs.
Base	Thickness =	1.00 ft.	Weight of Wet Well =	96,416.19 lbs.
Antifloatation Base	Diameter =	14.00 ft.	Weight of Base =	15,149.81 lbs.
Antifloatation Base	Thickness =	2.00 ft.	Weight. of Antifloatation Base =	15,881.79 lbs.
Depth of Wet We	ll embedded		Total Weight of Wet Well =	142,597.61 lbs.
into Antifloat	ation Base =	2.00 ft.	-	
Volume o	of Top Slab =	101.00 cu. ft.	Soil Weight Above Antifle	oatation Base
Volume of	Wet Well =	2890.58 cu. ft.	Volume of Soil =	1462.18 cu. ft.
Volun	ne of Base =	101.00 cu. ft.	 Weight of Soil =	153,529.24 lbs.
Vol. of Antifloat	ation Base =	105.88 cu. ft.	-	
Total Vol. of	Wet Well =	3198.46 cu. ft.	Anti-Buoyant Force of Wet Well =	145,566.01 lbs.
Buoyant Force of	Wet Well =	199,583.92 lbs.	Factor of Safety =	0.73

APPENDIX 14 - PORTER RIDGE PUMP STATION - FLYGT NP 3153 PUMP



Number of blades

2

Max. fluid temperature

40 °C

Project Block	Xylect-20620257	Created by	Dan Joyce 9/16/2024 Last undate	9/16/2024
		cicated on	5/10/2024 Last upuale	5/10/2024

Technical specification

Motor - General

Motor number	Phases	Rated speed	Rated power		
N3153.185 21-18-4AA-W 20hp	3~	1755 rpm	20 hp		
ATEX approved	Number of poles	Rated current	Stator variant		
No	4	26 A	5		
Frequency	Rated voltage	Insulation class	Type of Duty		
60 Hz	460 V	Н	S1		
Version code					
Motor - Technical					
Power factor - 1/1 Load	Motor efficiency - 1/1 Load	Total moment of inertia	Starts per hour max.		
0.83	87.5 %	2.38 lb ft ²	30		
Power factor - 3/4 Load	Motor efficiency - 3/4 Load Starting current, direct starting				
0.77	89.0 %	148 A			
Power factor - 1/2 Load	Motor efficiency - 1/2 Load Starting current, star-delta				
0.66	89.0 %	49.3 A			

Project Block

Program version 74.0 - 7/1/2024 (Build 136)

Xylect-20620257

Dan Joyce Created by Created on 9/16/2024 Last update

9/16/2024



a **xylem** brand

Data version 8/29/2024 13:07 A8P8

Usergroup(s) Xylem:USA-INT



Data version 8/29/2024 13:07 A8P8

Duty Analysis



VFD Curve



a xylem brand $Curves\ according\ to:\quad Water,\ pure\ , 39.2\ ^\circ F, 62.42\ lb/ft^3, 1.6891E-5\ ft^2/s$ [ft] Head 135 130 125 120 115 110 105 100 95 90-85 80 71.8% 75 70 65 60-55-71.8% 50-45 71.8% 40 35 71.8% 30-462 276mm 25 50 Hz 20-45 Hz 15 40 Hz 10 5 0-Overall Efficiency [%] Efficiency 60 50 40 Hz 45 Hz 50 Hz 40 Hz 45 Hz 50 Hz -462 276mm -55 ¥, 40-462 276mm 30 20 10-[hp] Pow er input P1 462 276mm (P1) 20 Shaft pow er P2 -462 276mm (P2) 16 -55 Hz -55 Hz 12-==58 Hz -<u>45 Hz</u> 8-40 HZ 4 [ft] NPSHR-values 462 276mm 40 35 30 . NPSHR = 32.809 ft 25 20 15 10-5-

 0
 100
 200
 300
 400
 500
 600
 700
 800
 900
 1000

 Nominal (mean) data shown. Under and over-performance from this data should be expected due to standard manufacturing tolerances.
 Please consult your local Flygt representative for performance guarantees.

 ect
 Xylect-20620257
 Created by
 Dan Joyce

1200 [US g.p.m.] Curve: ISO 9906 1100 0



VFD Analysis





VFD Analysis



Dimensional drawing





Usergroup(s) Xylem:USA-INT
APPENDIX 15 - FIELDSTONE PUMP STATION - FLYGT NP 3202.185 HT PUMP



APPENDIX 16 - ALTERNATIVE 2 LIFE CYCLE COST ANALYSIS

		Life	Cycle Cost An	alysis			
	Sanctu	uary at S	outhgate Phas	e İl Developm	ent		
Alternative 2	- Off-Site	Gravity S	Sewer Connect	tion to Porter	Ridge Pump Station		
New Gravity Sanitary Sewer Line							
Inputs and Assumptions					O&M Costs (% of Capital for Gravity Systems)	1%	
Planning Period	20	Years			10-year Items (% of Total for Gravity Systems)	5%	
Discount Rate	1.55%				20-year Items (% of Total for Gravity Systems)	0%	
Inflation Rate	3.20%				50-year Items (% of Total for Gravity Systems)	95%	
Initial Capitol Investment							
Item	Quantity	UOM	Cost Per Unit	Cost]		
8" PVC Gravity Sanitary Sewer Line	7100	LF	\$80	\$568,000]		
Manholes	23	EA	\$5,000	\$115,000			
Clearing & Grubbing	10	AC	\$7,500	\$75,000			
Temporary Construction Easement Acquisition	10	AC	\$50,000	\$500,000			
Sanitary Sewer Easement Acquisition	5	AC	\$100,000	\$500,000			
			Total	\$1,758,000			
Annual Costs							
Yearly Cost of Gravity System O&M	\$6,830						
Total Annual Costs NPV	\$157,450						
Life-Cycle Replacement Costs							
Cost of 10-Year Items at Year 0	\$34,150						
Cost of 10-Year Items at Year 10	\$46,794						
NPV of 10-Year Items at Year 10	\$40,123						
Cost of 10-Year Items at Year 20	\$64,119						
NPV of 10-Year Items at Year 20	\$47,140						
Cost 20-Year Items at Year 0	\$0						
Cost of 20-Year Items at Year 20	\$0						
NPV of 20-Year Items at Year 20	\$0						
Total Life-Cycle Replacement Costs NPV	\$87,262						
Residual Values							
Cost of 10-Year Items at Year 20	\$64,119						
Cost of 20-Year Items at Year 20	\$0						
Residual Value of 50-Year Items at Year 20	\$389,310						
Total Life-Cycle Replacement Residual Value at Year 20	\$453,429						
Total Residual Value NPV	\$333,358						
Total Net Present Value	\$1,669,354.4	7					

	Sanctu	ary at So	outhgate Phase	I Developme	ent	
Alternative	2 - Off-Site 0	Gravity S	Sewer Connecti	on to Porter R	Ridge Pump Station	
	Po	rter Ride	ne Pump Statio	n Upgrades		
Inputs and Assumptions				ii opgiaace		
Planning Period	20	Years			O&M Costs (% of Capital for Pump Stations)	3%
Discount Rate	1.55%				10-vear Items (% of Total for Pump Stations)	5%
Inflation	3.20%				20-year Items (% of Total for Pump Stations)	60%
					50-year Items (% of Total for Pump Stations)	35%
Initial Capitol Investment						
Item	Quantity	UOM	Cost Per Unit	Cost		
Porter Ridge PS Upgrades	1	LS	\$430,000	\$430,000		
			Total	\$430,000	J	
Annual Costs						
Floatrian Cost	¢0.09					
Electrical Cost Porter Ridge PS - Elvat NR 3153 HT 3~ 462	φ 0.0 6	KVVIT				
Pump On Time Per Cycle (min)	9.29					
Pump Cycles Per Hour	6.46					
Ave Daily Flow Rate (GPM)	105.26					
US MG / Year	55.34					
Pump Spec Energy (kWh/US MG)	660					
Yearly Cost of Electricit	v \$2.921.79					
Yearly Cost of Pump Station O&	\$ 12.900.00					
Total Yearly Costs at Year	0 \$15 821 79					
Total Annual Costs NP	\$364,735.14					
Life-Cycle Capital Replacement Costs						
Cost 10-Year Items at Year 0	\$21,500.00					
Cost 10-Year Items at Year 10	\$29,460					
NPV of 10-Year Items at Year 1	0 \$25,260.16					
Cost 10-Year Items at Year 20	\$40,367.55					
NPV of 10-Year Items at Year 2	0 \$29,677.95					
Cost 20-Year Items at Year 0	\$258,000.00					
Cost 20-Year Items at Year 20	\$484,410.62					
NPV of 20-Year Items at Year 2	0 \$356,135.36					
Total Replacement Costs NP	\$411,073.47					
Desidual Values						
Residual values	\$40.269					
Cost 20 Veer Items at Veer 20	\$40,308 ¢404.444					
Cusi 20-1 cal nellis at 1 cal 20 Residual Value of 50-Vear Items at Vear 20	ቅ404,411 \$00 300					
Total Life-Cycle Replacement Residual Value at Vear 20	\$615.079					
	\$452.201					
	ψ+52,201					
Total Net Present Value	\$753,607.36					

		Life	Cycle Cost Ana	lysis		
	Sanctua	arv at So	outhoate Phase	I Developme	ent	
Alternative 2	- Off-Site G	ravity S	ewer Connecti	on to Porter F	Ridge Pump Station	
Alternative 2	Ei/	aldeton	Dumn Station	Ungrados		
Innuts and Assumptions	1 1	FIUSION	e Fump Station	opgrades		
Planning Pariod	20	Voore			OSM Costs (% of Capital for Pump Stations)	20/
	1 55%	rears			10 year Items (% of Total for Pump Stations)	5%
Inflation	3 20%				20-vear Items (% of Total for Pump Stations)	60%
innauon	0.2070				50-year Items (% of Total for Pump Stations)	35%
Initial Capitol Investment						
Item	Quantity	UOM	Cost Per Unit	Cost]	
Fieldstone PS Upgrades	1	LS	\$642,000	\$642,000		
			Total	\$642,000	J	
Annual Costs						
Electrical Cost	\$0.08	k/\//H				
Fieldstone PS - Flygt NP 3202 185 HT	ψ0.00					
Pump On Time Per Cycle (min)	10.64					
Pump Cycles Per Hour	5.64					
Ave Daily Flow Rate (GPM)	215.31					
US MG / Year	113.19					
Pump Spec Energy (kWh/US MG)	660					
Yearly Cost of Electricity	\$5,976.17					
Yearly Cost of Pump Station O&M	\$19,260.00					
Total Yearly Costs at Year 0	\$25,236.17					
Total Annual Costs NPV	\$581,761.96					
Life-Cycle Capital Replacement Costs						
Cost 10-Year Items at Year 0	\$32,100.00					
Cost 10-Year Items at Year 10	\$43,985					
NPV of 10-Year Items at Year 10	\$37,714.01					
Cost 10-Year items at Year 20	\$60,269.69					
NPV of 10-Year items at Year 20	\$44,309.86					
Cost 20-Year Items at Year 0	\$385,200.00					
Cost 20-Year items at Year 20	\$723,230.31					
NPV of 20-Year items at Year 20	\$031,718.38					
Total Replacement Costs NPV	\$013,742.25					
Residual Values						
Cost 10-Year Items at Year 20	\$60,270					
Cost 20-Year Items at Year 20	\$723,236					
Residual Value of 50-Year Items at Year 20	\$134,820					
Total Life-Cycle Replacement Residual Value at Year 20	\$918,326					
Total Residual Value NPV	\$675,147					
Total Net Present Value	\$1,162,357,23					